

Chapter 6

6-1

Circular Motion & Other Applications of Newton's Laws

— Just more examples with
some interesting special cases

But
now with
forces
— the dynamics.

- uniform circular motion
- not so uniform circular motion.
- non-inertial frames
& inertial forces. (we already
anticipated ~~with~~ this
with the elevator problem.
- Resistive media
- a differential equation and
relation.

§ 6.1

Recall our general expression
for acceleration in polar
coordinates

6-2

$$\underline{a} = \left(\frac{d^2 r}{dt^2} - r \omega^2 \right) \hat{r} + \left(2 \frac{dr}{dt} \omega + r \frac{d\omega}{dt} \right) \hat{\theta}$$

$$\begin{aligned} v_{\text{tan}} &= r\omega \\ &= r \frac{d\theta}{dt} \\ &= \frac{ds_{\text{tan}}}{dt} \end{aligned} \quad \text{where } \omega = \frac{d\theta}{dt} \quad (\text{French-557})$$

If r is fixed for circular motion

$$\frac{dr}{dt} = 0, \quad \frac{d^2 r}{dt^2} = 0$$

$$\underline{a} = \underbrace{(-r\omega^2)}_{a_{\text{centripetal}}} \hat{r} + \underbrace{\left(r \frac{d\omega}{dt} \right)}_{a_{\text{tan}}} \hat{\theta}$$

$$\begin{aligned} \underline{a}_c &= -r\omega^2 \hat{r} \\ &= -\frac{v^2}{r} \hat{r} \end{aligned}$$

$$a_c = \frac{v^2}{r} \text{ for just magnitude}$$

Well $F = ma$ tells us if there is ^{non-zero} acceleration, there must be a non-zero net force.

So For circular motion there must be a radial force component of magnitude

$$F_{\text{centripetal force}} = m \frac{v^2}{r}$$

→ this is the centripetal force.

Note the centripetal force is NOT a magic force that turns on when there is circular motion → it is a force requirement needed to cause circular motion.
— A real actual force must supply this force.

A homely analogy may help.
Say there is a truck that

6-7)

Delivers groceries.

— the truck's function is
(to deliver groceries

→ So it's a delivery truck
by function.

But by nature it could
be a GM, Toyota, or even
a Chrysler (though
this seems unlikely)

So the centripetal ~~man~~ "centripetal
force" describes what
the force does, not what
it is.

Or another perspective.

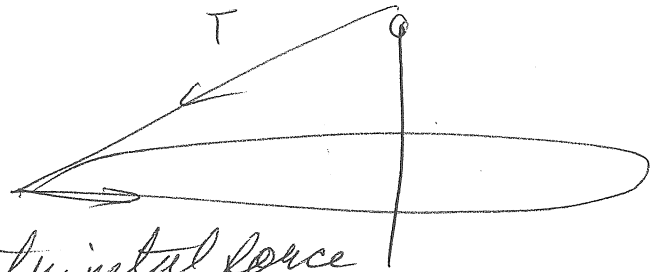
$$F_c = m \frac{v^2}{r}$$

is really mg
specialised for the radial
component of circular motion

Ex 6.1

(6-5)

— Conical pendulum
or sling.



- The string supplies the centripetal force
- it is a tension force

— DEMO. (students in front
a permitted to cover)



~~I can~~

3rd
law
story

{ Rope pulls on bob
bob pulls on rope
rope pulls on me
I pull on rope

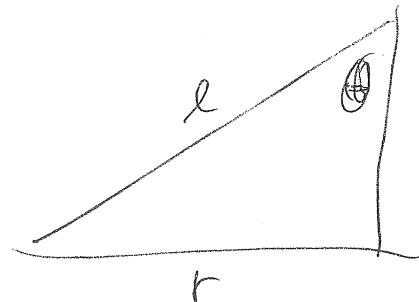
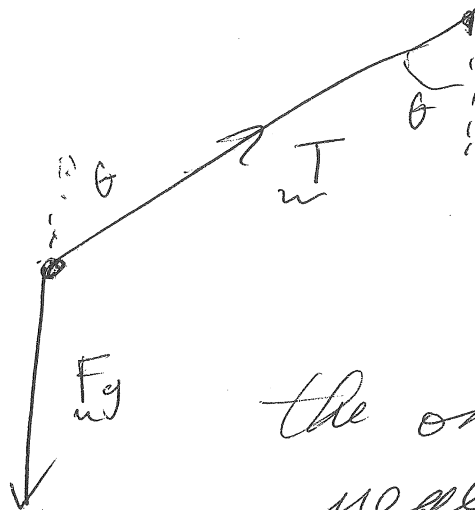
If there were no force to accelerate
bob into a circular motion, it
would fly off in a straight line

→ which is the whole point
of the sling as a weapon actually.

Let's analyse the forces
on the bob.

6-6

Bob as
point mass
in FBD



Class mentioned

the only two forces
neglecting air resistance.

$F=ma$ is always true and it's always
true component by component.

In r -direction $\sum F_r = -T \sin \theta = -m \frac{v^2}{r}$

$$T \sin \theta = m \frac{v^2}{r}$$

One could solve for T given
 $m, v, r, \sin \theta$

— Recall we don't have an intrinsic
force formula.

In y -direction $\sum F_y = T \cos \theta - mg = 0$

no
acceleration

$$\therefore T \cos \theta = mg$$

One can solve for angle by division

$$\tan \theta = \frac{v^2}{r g}$$

Note m canceled
out which often
happens in simple
gravity problems

$\tan \theta \sin \theta = \frac{v^2}{r g}$
 $\Rightarrow \theta^2 \approx \frac{v^2}{r g}$

because gravity is
~~a mass~~ linear in mass m
 and no it $F=ma$.

6-7

$$\theta = \tan^{-1}\left(\frac{v^2}{rg}\right)$$

This formula
 occurs in
 several different
 contexts with
 somewhat different
 meaning

or $\theta^2 = \frac{v^2}{rg}$ for small angle approximation

say $R = 5m$, $g = 9.8 m/s^2 \approx 10$

$$v = \frac{2\pi r}{\Delta t}$$

10 rings in Δt
 means $\Delta t = \dots$

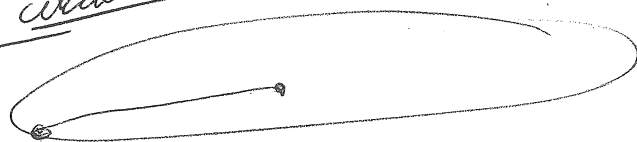
$$\approx \frac{6}{\Delta t}$$

$$\therefore \theta = \tan^{-1}\left(\frac{v^2}{rg}\right) \approx \sqrt{\frac{v^2}{rg}}$$

$$\theta = \frac{v}{\sqrt{rg}}$$

using small
 angle approximation.

Ex 6.2 Horizontal circular motion



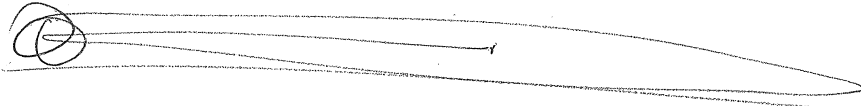
$$m = .5 \text{ kg}$$

$$r = 1.5 \text{ m}$$

cord breaks if $T > T_{\max} = 50 \text{ N}$
 How fast can the mass be
 swung before breaking?

6-8

$$T \sin \theta = \frac{m v^2}{r}$$



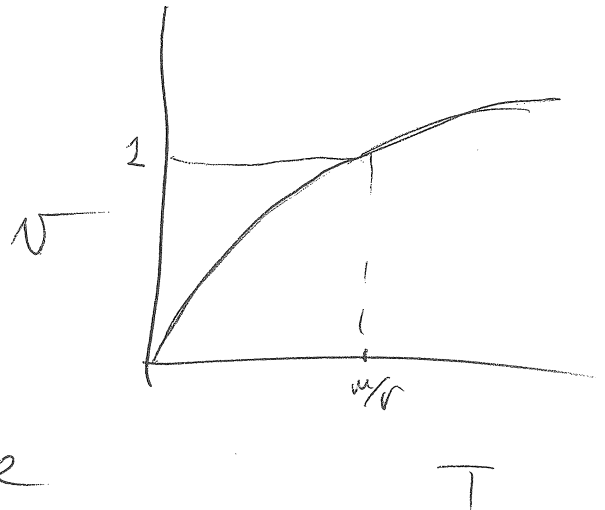
But say we are on a frictionless horizontal plane

$$\theta = 90^\circ$$

$$T = \frac{m v^2}{r}$$

$$v = \sqrt{\frac{T r}{m}}$$

v ^{strictly} rises with T .



$\therefore$ at $T_{\max}$, one gets $v_{\max}$

$$v_{\max} = \sqrt{\frac{50 \cdot 1.5}{.4}} = \sqrt{150}$$

$$\approx 12.5 \text{ m/s}$$

$$\underline{\text{Ans } 12.2 \text{ m/s}}$$

EG. 3 Car on a Horizontal Bend

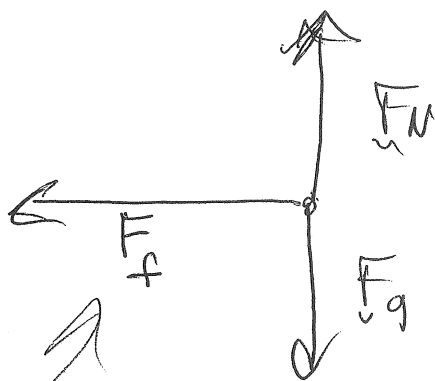
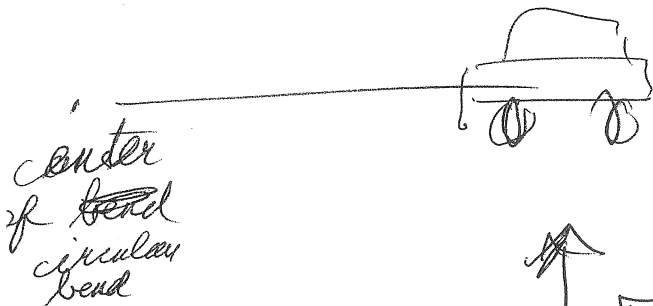
6-9

Such bends are rare
— because ^{road} designers almost
always bank roads for
very good reasons as we'll
soon see.

— Of course every ordinary
intersection is a small horizontal bend that you
take slowly for good reason also



Car moving into
the page



The only horizontal force on the
car is static friction

$$\sum F_y = F_N - mg = 0$$

$$F_N = mg$$

Static because
the wheels
are not
sliding on
road

Magnitude $F_f = \text{Min}(F_{\text{app}}, \mu_s F_N) = \text{Min}(F_{\text{app}}, \mu_s mg)$

6-10

v_{app} is the friction force you can supply to the ground in trying to turn

To be moving in a circle there must be a centripetal force

6-10

$$F_c = m \frac{v^2}{r}$$

Only friction can supply it.

But as $v \uparrow$ or $r \downarrow$
the force requirement gets bigger and the limit ~~increases~~

$$\mu_s m g = m \frac{v_{max}^2}{r} \quad \text{for a maximum bend or turn speed,}$$

~~D~~ mass cancels

and one solves for the limiting speed.

$$v_{max} = \sqrt{\mu_s r g}$$

μ_s r g
 0.523 35m 9.8 m/s²

Text here but elsewhere rubber on concrete is given as 1 — but this is rubber on asphalt.

$$\begin{aligned} &\approx \sqrt{.5 \cdot 35 \cdot 10} \\ &= \sqrt{175} \approx 13 \text{ m/s} \\ &= 13 \text{ m/s} \cdot \frac{1 \text{ mi}}{1609 \text{ m}} \cdot \frac{3600 \text{ s}}{1 \text{ h}} \\ &\approx 30 \text{ mi/h} \end{aligned}$$

This isn't very good actually

6-12

You can only go $\sim 30 \text{ m/h}$ around a bend and even this is pushing it to the safety limit. $\rightarrow$ Actually

— you'd have to go much slower to be safe especially if friction were reduced by water or ice.

the car becomes a bit hard to control if there



in a skid on a slippery roadway friction force on turned wheels?

~~This leads~~

⊙ This leads to banking

Ex 6.4

— You know road bends are usually banked and empirically you sort of know why. in part gravity ^{& normal force} is available to help supply the centripetal force.

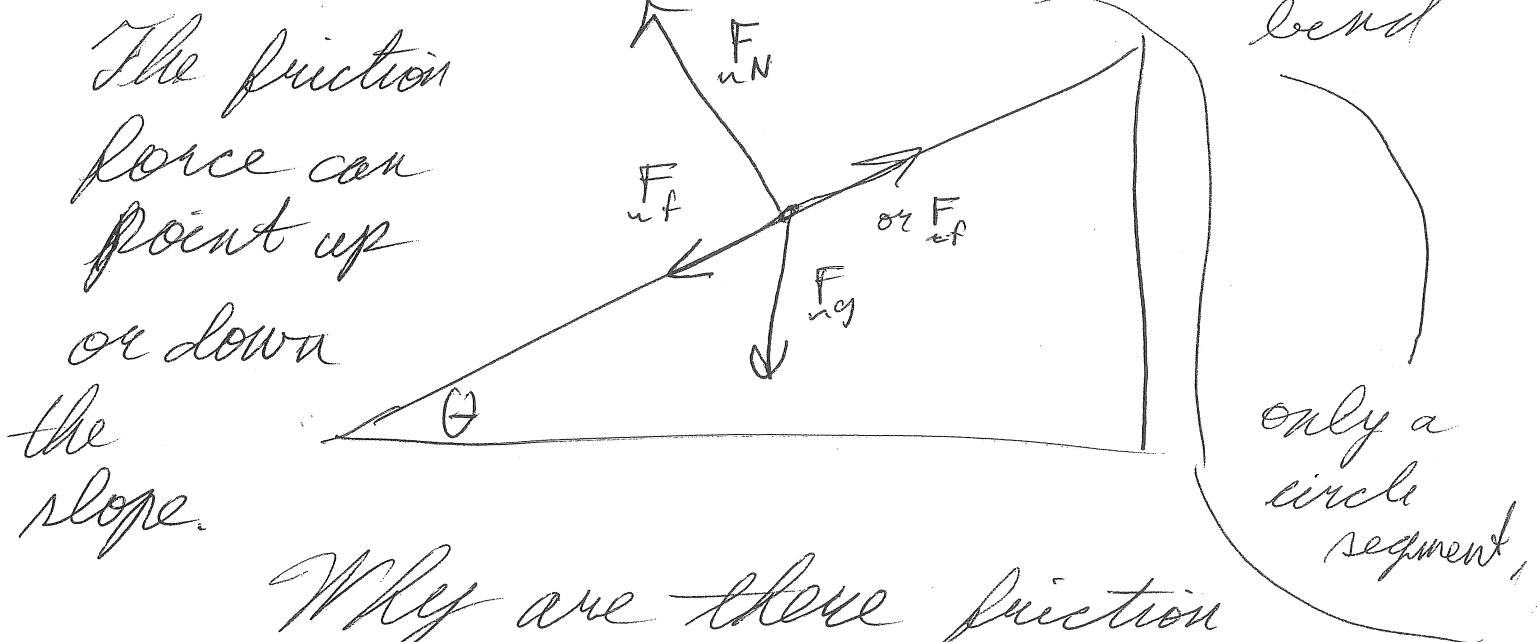
and you
to
a
low
round
edging
backed
or more.

~~force~~ But that's 6-13

only partially the reason why. The road normal force helps too.

Let's analyze the forces

Consider a circular bend



Why are there friction and normal forces?

~~The~~ Gravity (on the Earth's surface) is always turned on.

Static Friction is always helping to ^{change speed} ~~accelerate~~ and ~~decelerate~~, but that along the direction of travel.

Static Friction also ~~tries~~ tries to slow car

TM-130

6-19) The normal force helps against gravity — on level ground it ~~does~~ does all the support against gravity.

But if you are making a bend, the car is pushing outward on the road using the car's normal force and friction force and the road pushes back to accelerate the car ~~around~~ around the bend.

Joining
parts
with
wheel
—
slows
into
movement

But friction is not so trustworthy.

It can fail

It varies because of road conditions — wet, icy, dry

It's actually a bit hard on car and road.

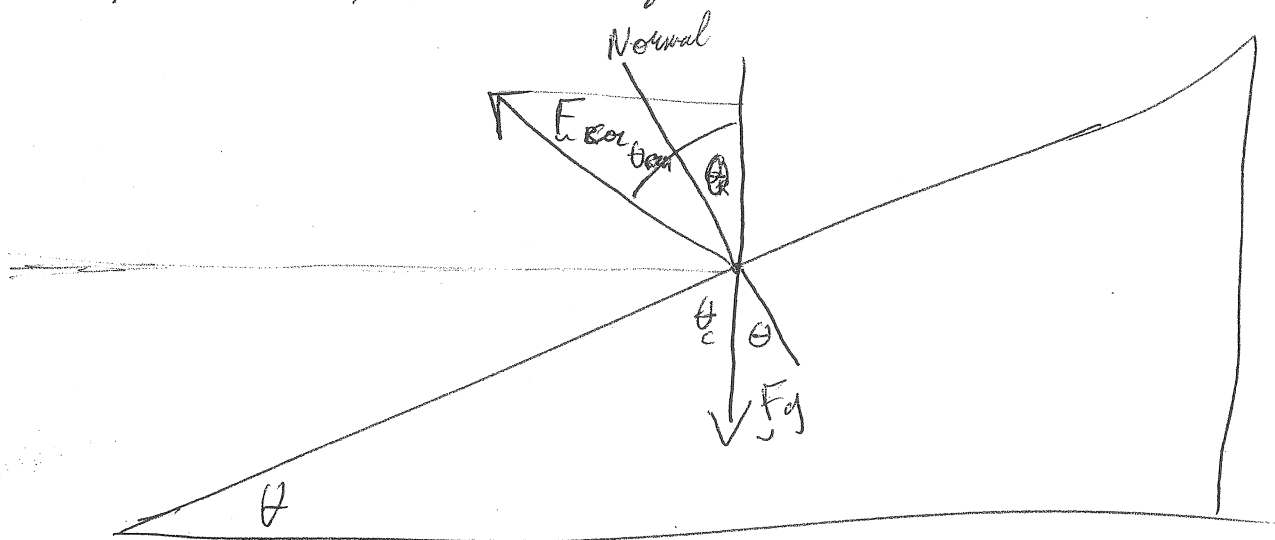
Car is a bit hard to control if strong ~~friction~~ sideways friction is demanded of the wheels. ? I sure think so.

So road designers would rather not rely on friction at all and one can bank the road so that this is the case.

Consider a banked curve 6-15
 and let's write

$$\vec{F}_{\text{contact}} = \vec{F}_f + \vec{F}_N$$

So we only consider the net road force.



Now if you are in fact making the bend, there must be a centripetal force ^(with in the net force of $F = ma$) only $\vec{F}_{\text{contact}}$ has a component in the center direction.

$$m \frac{v^2}{r} = F_{\text{con}} \sin \theta_{\text{con}}$$

6-1b)

There is no acceleration
in the ~~xy~~ direction.

$$\text{Thus } \text{may} = F_{\text{con}} \cos \theta_{\text{con}} - mg$$

$$\text{or } \cancel{mg} = F_{\text{con}} \cos \theta_{\text{con}}$$

to find θ_{con} just divide

$$\frac{v^2}{rg} = \tan(\theta_{\text{con}})$$

F_{con}
& m
miraculously
cancel
out

$$\text{or } \theta_{\text{con}} = \tan^{-1}\left(\frac{v^2}{rg}\right)$$

~~or~~ using the 2nd, we have
found what θ_{con} has to be
if the car is in fact making
the ~~over~~ bend.

Now we are road engineers
(civil engineers ^{who are you} or very very
polite engineers)

and we adjust ^{bank angle} $\theta = \theta_{\text{Ben}}$ 6-17

$$\therefore \theta = \theta_{\text{Ben}} = \tan^{-1}\left(\frac{v^2}{rg}\right)$$

In this case F_{Ben} is perpendicular or normal to the road.

Friction which is always parallel to the road can make no contribution to F_{Ben}

$$\text{and } F_{\text{Ben}} = F_N$$

Friction is never called upon and so can never fail if $\theta = \theta_{\text{Ben}}$

So even if the road were frictionless, the car would still make the bend.

But one must go at v specified.

6-18

Now one can't actually
have one banking angle

Too slow and ~~you~~ some friction
is needed to prevent sliding
in. $\rightarrow$ uphill friction

Too fast and some friction is needed
to prevent sliding out
 $\checkmark$ downhill friction.

Remember the ~~form~~ normal force
and the ^{static} friction forces are
both forces of reaction.

— they are as strong as they
need to be — until they
fail.

— ^{static} friction fails relatively
easily — and becomes kinetic friction

— the normal force of a
asphalt road doesn't fail easily ^{to road}
 $\hookrightarrow$ it takes a lot of ^{applied} force to ^{doesn't} seriously deform a road. ^{deform} ^{early}

Our analysis actually
applies to ^{all} the bits
and ~~inter~~ occupants of
the car.

6-19

— If you go at the ramp
speed (in our ideal case)
you don't have any tendency
to slide sideways in your seat.

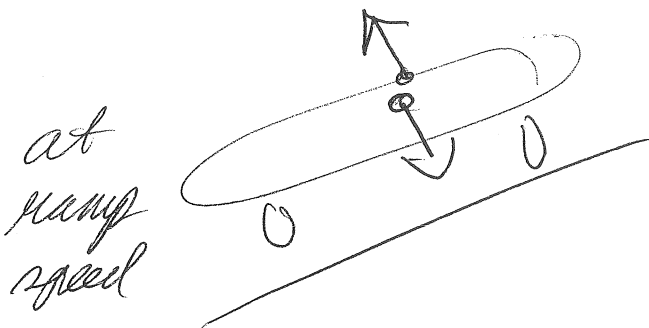
→ making a bend just pushes you
^{directly} ~~down~~ into the seat.

→ So the seat pushes
directly out.

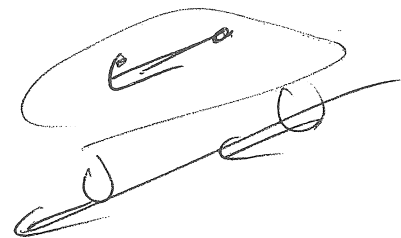
~~giving out~~ just the right normal force

Also only compression forces
act on car bits

rather than shear forces.



going
too fast
when



shear forces must
work.

6-20

- using

shear forces tend to be hard on a car.

Now there really can be only one ramp speed for practical driven reasons.

— but the banking angle θ must vary from 0 to $\theta_{\max}$ back to 0 in a quasi-continuous way

— So road engineers must vary v from $v_{\min}$ to $v_{\max}$

$$\theta = \theta_{\text{con}} = \tan^{-1}\left(\frac{v^2}{rg}\right)$$

in order for the road force to always be normal.

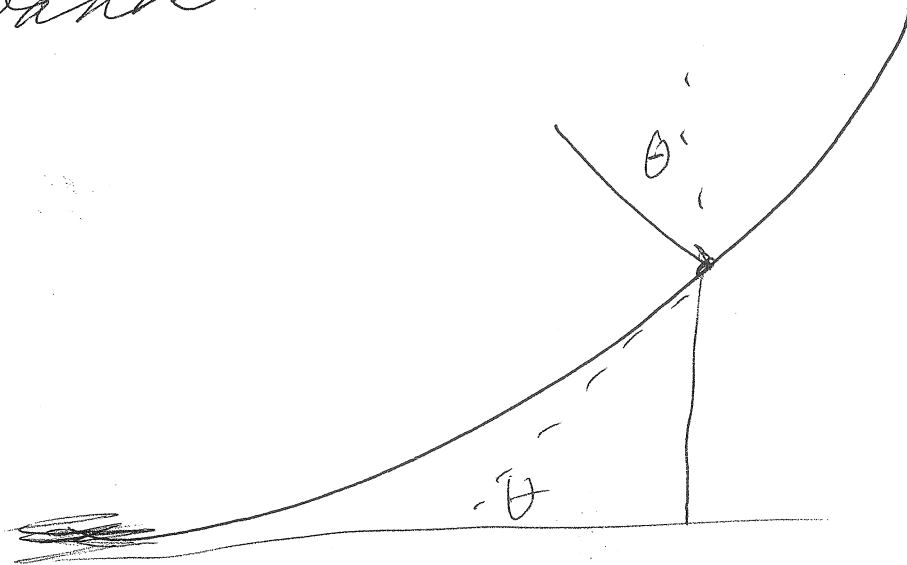
All the above is somewhat idealized

— road engineers must have other considerations but to first order they

must use $\theta = \theta_{\text{con}} = \tan^{-1}\left(\frac{v^2}{rg}\right)$ for banking.

There are ^{nearly} frictionless
and cases actually

- not for cars, of course,
but for bobsleds.
 - and for bobsleds there
is no specified speed.
 - the bobsledders want to go
as fast as possible — or so I
guess — maybe the slowest sled
wins? I've no idea.
- So the curves are continuously
bank



- Since there is no friction (ideally),
the sled will slide sideways up or down

6-22

~~until~~ until the
road force needed to
make the bed is all normal
force.

$$\therefore \theta = \tan^{-1}\left(\frac{v^2}{rg}\right)$$

— higher θ (for fixed v),
larger θ ,
higher up the slope the
sled rises.

All this you qualitatively
understand when you think
of it. — some for skate boards, but
except that a wheeled car.

Some values from our earlier
example

$$v = 13.4 \text{ m/s}$$

$$r = 35 \text{ m}$$

$$g \approx 10$$

$$\theta = \theta_{\text{Req}} = \tan^{-1}\left(\frac{v^2}{rg}\right)$$

$$\approx \tan^{-1}\left(\frac{180}{350}\right) \approx \tan^{-1}\left(\frac{1}{2}\right)$$

$\approx \frac{1}{2}$ radian using
the small
angle approx.

6-23

$$= \frac{1}{2} \text{ rad } 60 \left(\frac{\text{deg}}{\text{rad}} \right)$$

$$\approx 30^\circ \quad \underline{\text{ANS}} \quad 27.6^\circ$$

§ 6.2 Non-Uniform Circular Motion

In polar coordinates

$$\underline{a} = \left(\frac{d^2 r}{dt^2} - r \omega^2 \right) \hat{r} + \left(2 \frac{dr}{dt} \omega + r \frac{d\omega}{dt} \right) \hat{\theta}$$

For circular motion
but not uniform

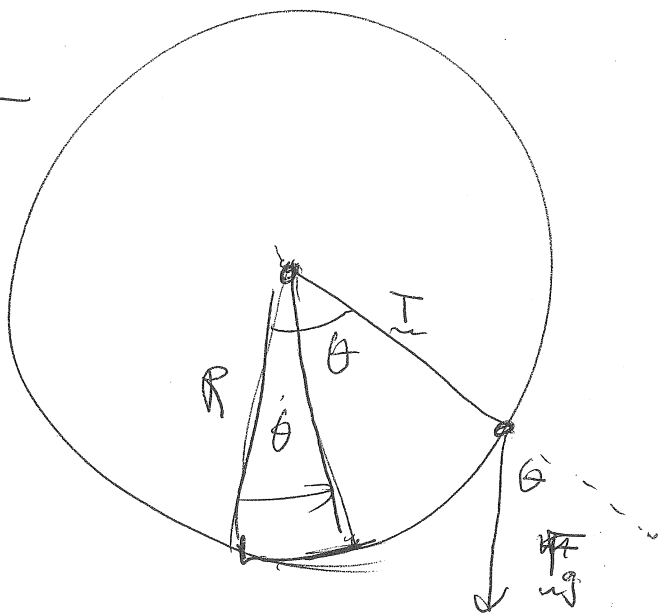
$$\underline{a} = \underbrace{(-r \omega^2)}_{a_c} \hat{r} + \underbrace{r \frac{d\omega}{dt}}_{a_{tan}} \hat{\theta}$$

$$a_c = r \omega^2 \quad \text{but } \omega = \frac{v}{r}$$
$$= \frac{v^2}{r} \quad \text{our usual magnitude formula.}$$

6-24

Just one exampleEx 6.6

Swing a bob
in a vertical
loop with a
string.



Measure θ positive
from vertical

$$ma = m \frac{v^2}{R} = F_c = T - mg \cos \theta$$

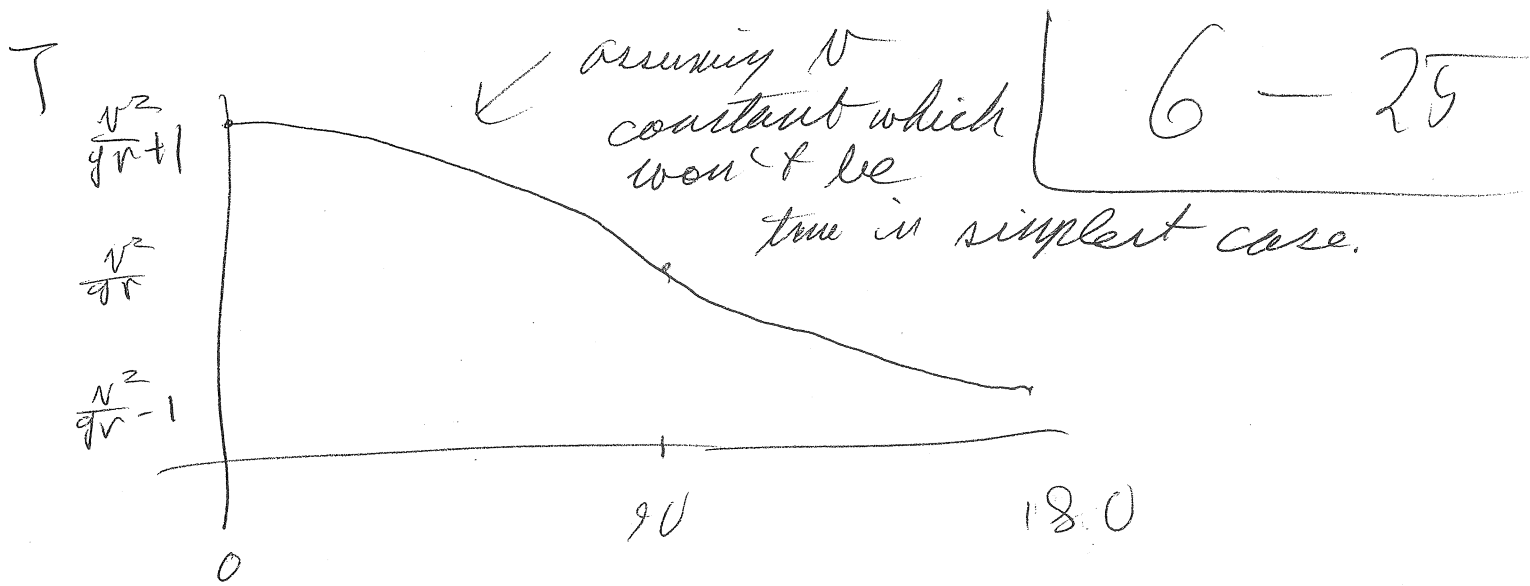
Taking positive
inward for
consistency
with text

$$T = mg \cos \theta + m \frac{v^2}{R}$$

$$= mg \left(\frac{v^2}{gr} + \cos \theta \right)$$

No ~~parameters~~ in this case

Tension
force from
Newton's 2nd
law and
gravity law.



No problem if $T \geq 0$ always.

But what if $T < 0$?

Well in deriving our tension rule we assume tension would always be adequate to circular motion.

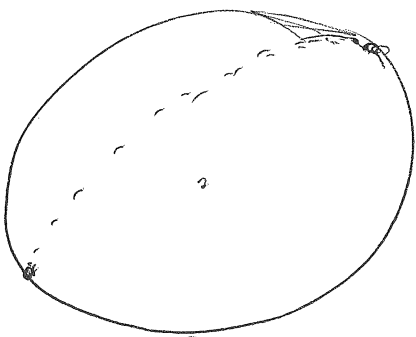
— this is true for stretching force for our ideal string.

But ~~one~~ can't push on a string (at least on ideal one).

When T goes to zero the bob will go into parabolic flight.

6-26

Something like this



Leaving and rejoining the circular path is NOT symmetrical in general

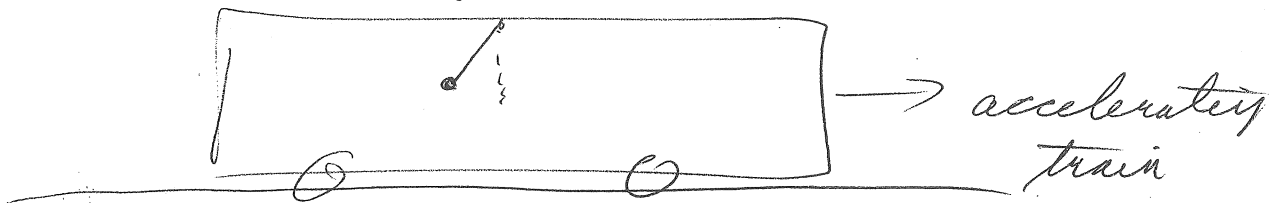
Proof is tricky
see SJ-144

§ 6.3 Non-Inertial Frames & Inertial Forces

We already considered the elevator case in Ch. 5 notes
(I went a bit beyond ^{SS} there).

Ex 6.7

Train case on an elevator on its side.



$$F_{\text{net}} = m \underline{a}$$

always true but referenced to an inertial frame.

In an accelerating train -
the y direction is normal.

6-27

First assume $a_{\text{train}} = 0$

Then for an object

$$\begin{aligned} v_{\text{rel}} &= v_{\text{ground}} - v_{\text{train}} \\ a_{\text{rel to train}} &= a_{\text{rel to ground}} \end{aligned}$$

Not derivations here, but prime from other frame.

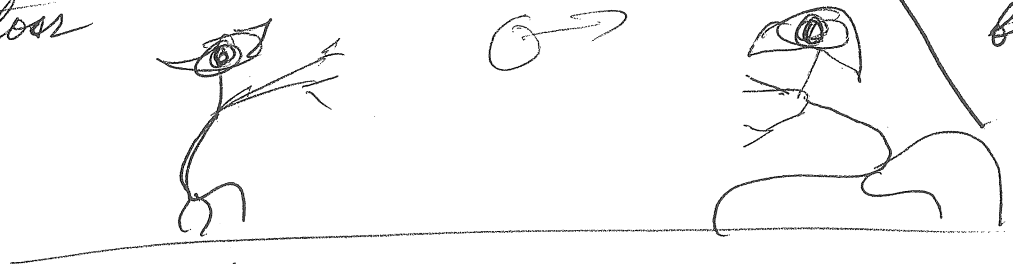
$$F_{\text{net}} = m a_{\text{rel}}$$

same

These means all forces give the same acceleration in both ground and train frame.

is fine either relative to train or ground.

Say you play toss



$$v_{\text{rel}} = v_{\text{ground}} - v_{\text{train}}$$

for all objects.

calculate all kinematics in train frame.

Everything is perfectly normal.

and $a_{\text{rel}} = a_{\text{train}}$

$$v_{\text{rel}} = v_{\text{ground}} - v_{\text{train}}$$

$$\text{or } v_{\text{ground}} = v_{\text{rel}} + v_{\text{train}}$$

6-28

So all mechanical experiments like toss are the same in train as relative to ground.

$F=ma$ predicts the same results, same kinematics except for additive constants of integration.

To get ground ~~let~~ velocities, just add v_{train} .

Review your whole life experience in trains, planes, and automobiles.

when these ~~accelerations~~ don't accelerate relative to the ground everything is normal.

Remember play toss with your little in the back seat stuff.

But when ^{the train} ~~one~~ accelerates things are a bit different.

Say it is all horizontal x acceleration — so nothing funny in y -direction.

a_{xt} and nothing forbids

us from ~~let~~

$$a_x = a'_{x,t} + a_{xt}$$

$$\text{or } a'_{x,t} = a_x - a_{xt}$$

} Relative acceleration.

Now $F_{x \text{ net}} = m a_x = m(a'_{xt} + a_{xt})$

$F_{x \text{ net}} - m a_{xt} = a_{xt}$

define as a new
field force $F_{\text{inertial}} = -m a_{xt}$

— like a sideways
gravity field force.
A new inertial or fictitious
force.

$F'_{\text{net}} = m a'_{xt}$

just $F = ma$ relative to train
with the new fictitious
or inertial force $-m a_{xt}$

Say $F_{\text{net}} = 0$ or $F'_{\text{net}} = -m a_{xt}$
only.

Then $-m a_{xt} = m a'_{xt}$

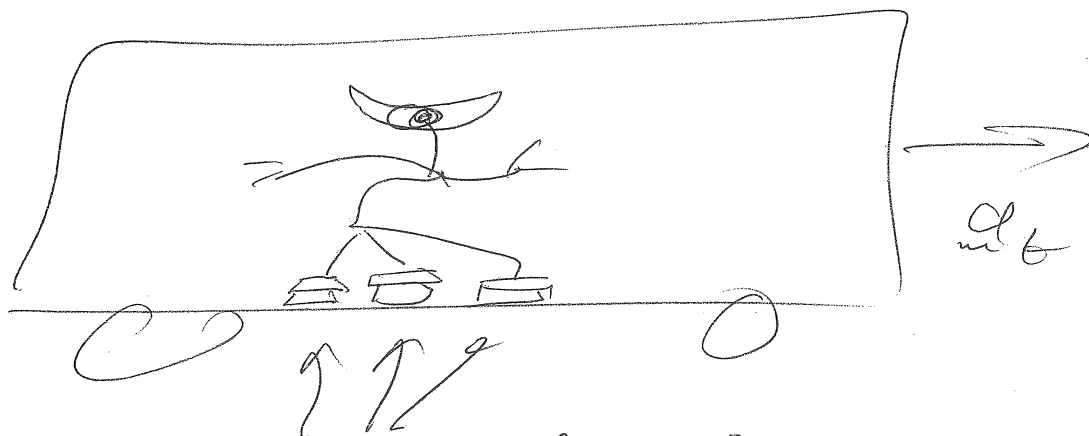
$a'_{xt} = -a_{xt}$

So an object without
any real forces would accelerate

6-30)

in the train frame
even though unaccelerated
in the ground frame.

- but it's a field force
~~not a~~ or a body force.
- it "pulls" atom by
atom



frictionless ice

- the alien would slide back
freely with $a_{is} = -a_{0t}$
- no stress or strain as long
as he doesn't try to resist.
- if he does it's like fighting
sideways gravity.

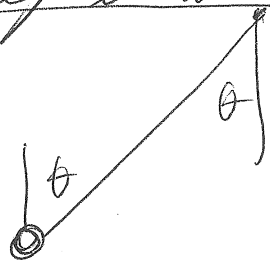
You know the sideways gravity effect from being in ~~cars~~ cars when they accelerate.

6-31

— you don't feel the inertial force $\rightarrow$ there is no force to feel

$\rightarrow$ What you feel is the strain in your muscles of accelerating yourself to go with the train.

Hanging object at rest in an accelerating train. done problem before on a truck.



In train frame

prime relative to ground

$$\underline{a} = 0$$

$$\sum F'_x = T \sin \theta - m a'_{xt} = 0$$

$$\sum F'_y = T \cos \theta - mg = 0$$

Just divide to get.

$$\tan \theta = \frac{a'_{xt}}{g}$$

6-32

$$\theta = \tan^{-1}\left(\frac{a_{\text{rel}}}{g}\right)$$

Say $a_{\text{rel}} = 2 \text{ m/s}^2$

$$g = 9.8 \text{ m/s}^2 \approx 10$$

$$\theta \approx \tan^{-1}\left(\frac{2}{10}\right) = \tan^{-1}(.2)$$

$$\approx 2 \text{ rad in small angle approximation}$$

$$\approx 12^\circ$$

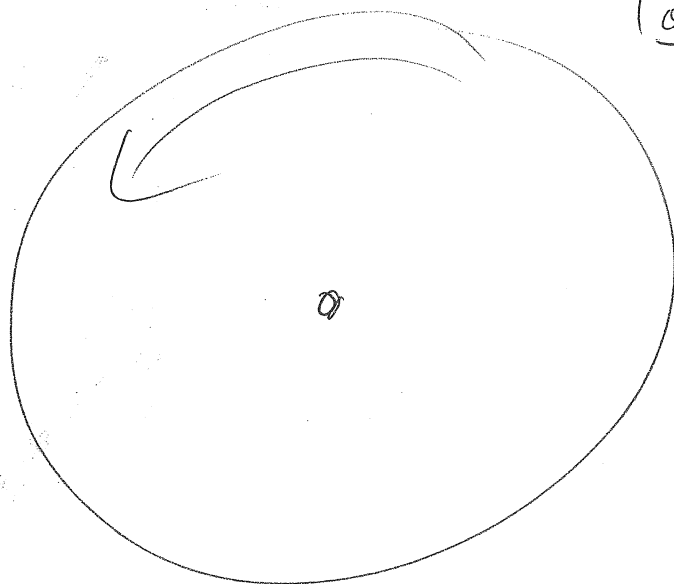
you could see this intuitively be some in the ground frame.

→ as in a hmk problem

Rotating Frames are trickier

Top view.

Non-Inertial Frames



To make

$F = ma$ work in a rotating frame requires two ~~more~~ inertial forces.

One is easy to derive

6-33

$$\underline{a'}_{\text{rel}} = \underline{a} - \underline{a}_c$$

↑
centripetal acceleration

$$\underline{F}_{\text{net}} = m \underline{a} = m \underline{a'}_{\text{rel}} + m \underline{a}_c$$

Define $\underline{F'}_{\text{net}} \equiv \underline{F}_{\text{net}} - m \underline{a}_c = m \underline{a'}_{\text{rel}}$

$$\underline{a}_c = -\frac{v^2}{r} \hat{r}$$

Not a
general
formula.
Really just
for confined
to a plane

$\therefore$ Define $\underline{F'}_{\text{inertial}} = -m \underline{a}_c = m \frac{v^2}{r} \hat{r}$

This is the centrifugal force.

— the force that tries to throw
you off merry-go-rounds
and carnival centrifuges.

If you are at rest in the rotating
frame, forces are balanced
and

$$\underline{F'}_{\text{net}} = \underline{F'}_{\text{centripetal}} + \underline{F'}_{\text{centrifugal}} = 0.$$

6-34

Actually our derivation above is slightly faulty due to subtle reasons.

omit?

$$\underline{a_{rel}} = \underline{a} - \underline{a_c}$$

is the relative acceleration

in a sense it's what one thinks of when one defines relative acceleration

but it's not the acceleration measured in the rotating frame

— rotating frames are tricky.

When you do the analysis carefully you find

(which we won't do and most books seem to muck it up)
 — it takes a few pages, Symon 3rd, 27.
 — get the right result but ~~lose~~ ^{does} lose some reasoning & faultily it seems to me.
 Fred 571 mucks it.

$$\underline{a} = \underline{a}' + \underline{a}_{centrifugal} + \underline{a}_{Coriolis}$$

relative to inertial frame

acceleration measured in rotating frame

centrifugal acceleration

Coriolis acceleration that depends on $\underline{v}$

the velocity in the rotating frame.

If the body is at rest
in the rotating frame,
 $a_{\text{coriolis}} = 0$

6-35

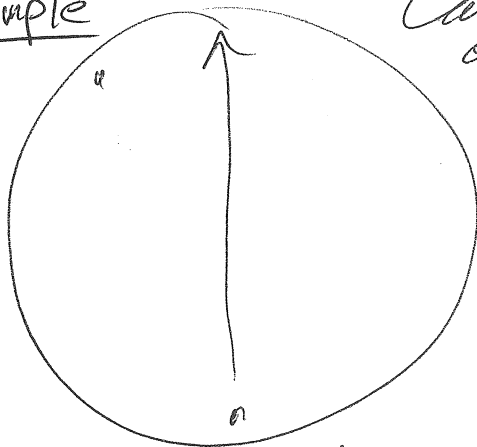
$$F_{\text{centrifugal}} = -m a_{\text{centrifugal}} = m \frac{v^2}{r} \hat{r}$$

$$F_{\text{coriolis}} = -m a_{\text{coriolis}}$$

I won't ~~repeat~~ write it out
— it's not so bad, but it's beyond
our scope.

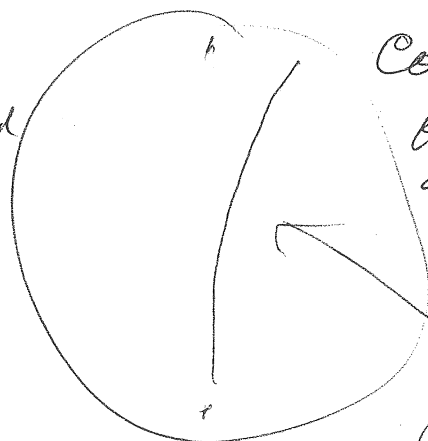
But the Coriolis force in
action is easy to notice
and understand in simple cases.

Example



ground
frame

Playmex
Caught
on a
rotating
merry-go-round

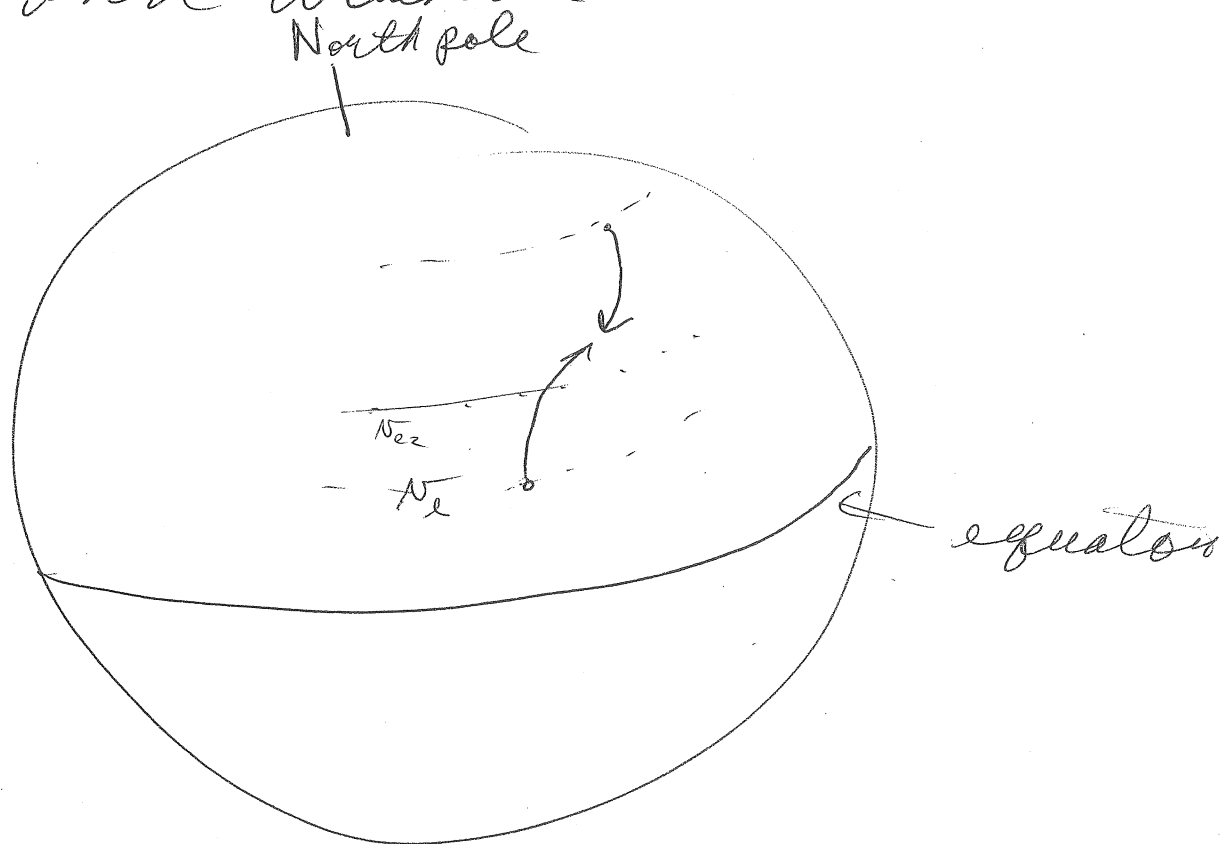


rotating
frame

Coriolis
force
deflection.

A "force"
causes the
deflection

6-36) The Coriolis force
is important in climate
and weather



$$N_{e2} < N_e$$



ω is the same
at all latitudes,
but

— so a wind blowing north
tends to deflect to the east
and one blowing south deflects
to the west.

This gives rise to cyclones and
anticyclones in weather.

Northern Hemisphere

Cyclones

anticyclones

6-37

low
pressure

high
pressure

swirl counterclockwise

clockwise
swirl.

most powerful
are hurricanes/typhoons

In the southern hemisphere everything
is mirrored. (or mirror image).

6-38

§6.4 Motion in Resistive

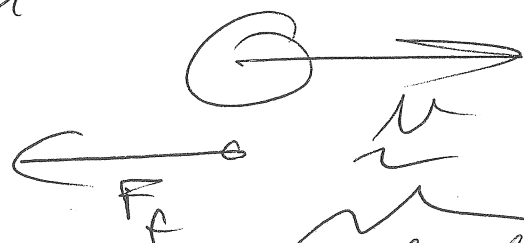
Media or Drag

→ i.e., fluids which are comprised of both liquids and gases

The resistive forces oppose motion

and are usually velocity

dependent.



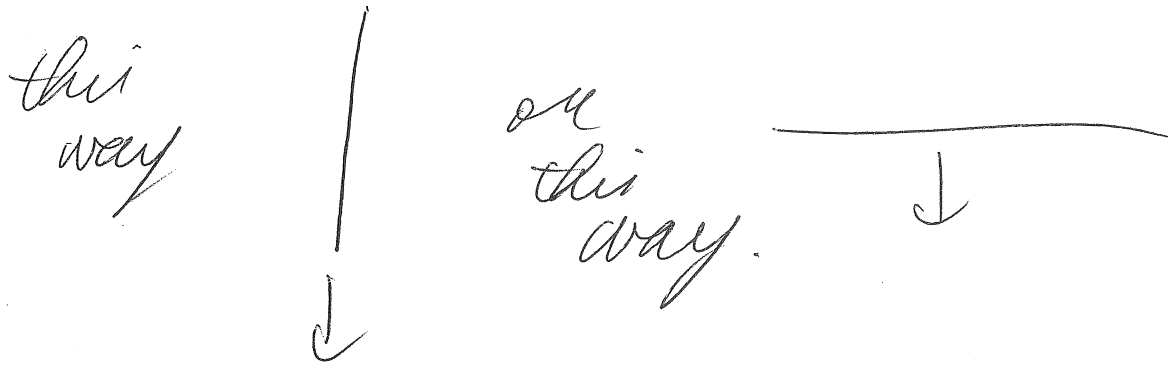
velocity
relative to
fluid. object

→ in detail in a very complex fashion that depends on velocity, shape, orientation, texture, rigidity of moving body.

moving
or
fluid
moving relative
to outside
world.

For orientation
effect consider a sheet
of paper dropped

6-39



But there are a couple of
very useful approximate
laws — that in some
cases are quite exact.

→ They are simple enough to
allow ~~some~~ some analysis
of how ~~they~~ ^{resistance} affects
motion

6-40

French 210 AF

Case 1: A linear resistive drag
(Stokes Drag)

~~force~~

$$\vec{F}_R = -b \vec{v}$$

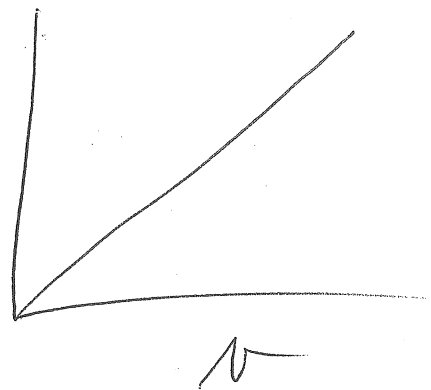
velocity of body

points
opposite
to motion

a constant depending
on shape, orientation
texture, ... of object

$$b > 0$$

The
resistive
force magnitude
increases
linear with



vel speed.

This force law is most appropriate
for relatively low speeds.
of small objects

To analyze how this force

Consider a body of mass m sinking under the gravitational force.

6-41

Say y down y is positive

~~no~~ no forces in the x -direction.

We will neglect the buoyancy force which for simplicity $F_b = m_{dis} g$ upward
Serway - 396 which

$$\sum F_y = mg - bV = ma$$

Note b is mass independent but $D = \frac{b}{m}$

or

$$ma + bV = mg$$

$$\frac{dV}{dt} + \frac{b}{m}V = g$$

D has units of inverse time

so that $\frac{dV}{dt}$ and DV have same units.

Just effectively change gravity g to $(m - m_{dis})g$ & g actual

In fact $b \sim$ Area cross section $\propto PA_{cl} \propto \frac{1}{2} \rho v^2 A_{cl}$ to motion direction

or objects $\frac{1}{2} \rho v^2 A_{cl}$ $\frac{1}{2} \rho v^2 A_{cl}$ $\frac{1}{2} \rho v^2 A_{cl}$

$$D = \frac{b}{m}$$

resistive effect $\propto \frac{1}{2} \rho v^2 A_{cl}$

This for some of you may be your first example of a differential equation (DE)

3. upper density, the smaller it is which is non trivial

B. if it does change inner mass

6-42

An equation
whose solution is not
a number, but a
function (e.g. $V(t)$) of
an independent
variable (e.g., t)

and where the function and
~~has~~ various orders of derivatives
appear in the equation.

D $\mathcal{E}$ s are in fact everywhere
in physics and in life

— In fact much of the numerical
science and engineering amounts
to solving D $\mathcal{E}$ s.

→ including economics (not that you'd
ever know it,

This is a 1st order D $\mathcal{E}$

— since the highest derivative
of V is $\frac{dV}{dt}$ the 1st order
derivative.

— it is also linear

6-43

since v and $\frac{dv}{dt}$

occur linearly in the DE.

— It has a driven term g which is not multiplied

This DE is analytically ^{by v} or solvable.

$$\frac{dv}{dt} + Dv = g$$

We'll do that solution
(and go just a bit
beyond the text.)

But first a few
simple results.

We will assume
the object starts from
rest.

~~so $v(0) = 0$~~ $v(t=0) = 0$

and then $\frac{dv}{dt} \approx g$ for t small
somehow.

a derivative
The g causes
the motion that
the resistive
force opposes.

If $b=0$, the
DE would reduce
 ~~$\frac{dv}{dt} = g$~~

$v = gt$ assuming
a trivial DE the
object starts
from rest.

6344

$$v \approx gt$$

for t small

→ just ~~grav~~ acceleration
under gravity.

But as the body accelerates
 v grows and so does

Dv .

At some point ^{in time} one reaches
a terminal velocity v_T one
might guess
such that

$$Dv_T = g$$

where $\frac{dv}{dt} = 0$

$$v_T = \frac{g}{D}$$

$$\frac{1}{D} = \frac{v_T}{g}$$

Then $\frac{dv}{dt} = 0$ in the DE.

No further acceleration happens.
One would guess
— the

The DE is then solved 6-45
if N stays constant at N_T

$$\frac{dN}{dt} = 0 \text{ and } DN_T = g.$$

→ The actual solution of the DE
verifies if and when this happens.

Omit?

OK let's solve the DE

$$N' + DN = g$$

The trick is to use an integrating factor f
which is initially unknown.

It is a
function
of t .

$$fN' + fDN = fg$$

We demand that

$$(fN)' = fN' + fDN$$

$$f^2 N' + f' N$$

by chain rule.

6-76

So our demand becomes

~~$$f'v = fDv$$~~

$$f'v = fDv$$

$$\text{or } f' = fD$$

$$\frac{df}{dt} = fD$$

$$\frac{df}{f} = D dt$$

and integrate
both sides

$$\ln f = Dt + \text{Const}$$

$$e^{\ln f} = e^{Dt + \text{Const}}$$

$$f = e^{Dt}$$

If you haven't
seen this
procedure before
just accept it.
as a foremanwhere we drop the
constant since the
overall scale of
 f is irrelevantNow we
have f

$$(fv)' = fg$$

$$fv|_0^t = g \int_0^t e^{Dt'} dt'$$

Integrate
both sides
with respect to t

e is
the
exponential
number or
Euler number
on base of
natural logarithms.

It's irrational
(bad, mad, and
dangerous to know)

$e = 2.71828...$
never repeats
- Can't be
expressed
as fraction

$$e^{Dt} N = g \frac{e^{Dt}}{D} \Big|_0^t$$

16-41

$$= \frac{g}{D} (e^{Dt} - 1)$$

$$N = \frac{g}{D} (1 - e^{-Dt})$$

or $N_T \rightarrow$

We can define $\tau = \frac{1}{D} = \frac{N_T}{g}$

time constant
or e-folding time in the
jargon I use ~~now~~

$$N = N_T (1 - e^{-t/\tau})$$

N_T for $t \rightarrow \infty$
only

$$N_T [1 - (1 - t/\tau)]$$

$$= N_T t/\tau$$

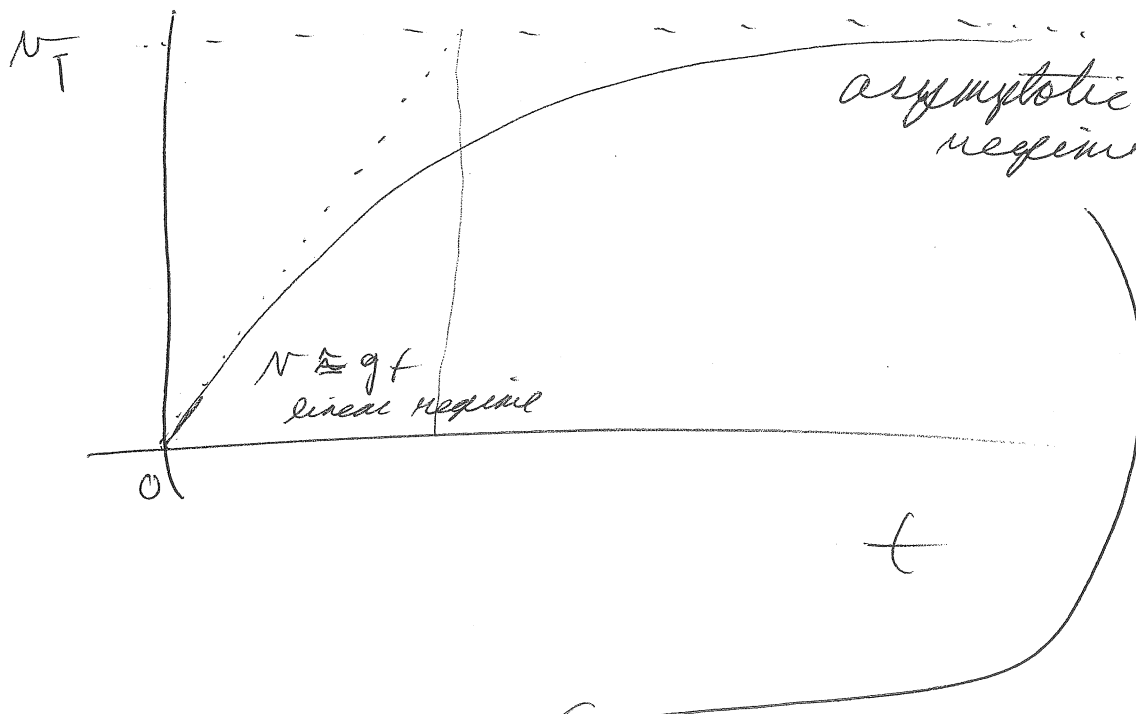
$$= \frac{g}{D} Dt$$

$$= gt$$

which is the
small t velocity behavior
we anticipated.

1st order Taylor
expansion
for small t
 $t/\tau \ll 1$

6-48



Characteristic means characterizing.
 - No precise meaning.
 - there is no sharp change in behavior between the two regimes

The object formally never reaches v_T in finite time.

~~At $t = \tau$~~ v just becomes asymptotic to v_T — always approaching.

The transition time between the two regimes ~~at~~ can be set at $t = \tau$

where $e^{-t/\tau} = e^{-1}$

Note if one just had linear increase then

at $t = \tau$, $v_{\text{linear}} = g\tau = \frac{g}{D} = v_T$

Actual $v(\tau) = v_T [1 - e^{-1}] = v_T \cdot 0.632$

You may wonder
 what ~~that~~ ^{N_T} actually means
~~that~~ in realistic not so idealized
 cases.

— In real cases there are always
 velocity perturbations of some
 size δv .

Small
 Greek deltas
 — meaning usually
 small change in

At some point
 the formal solution
 will have

$$|N_T - v| \leq \delta v$$

and often then
 one can say the
 velocity has reached
 N_T for practical
 purposes.

or if $|N_T - v|$ is smaller
 than some value you care to
 as a standard of ^{smallest} significance,

6-50

then for practical purposes velocity has reached

terminal for your purposes.

really in few falling times.

$$-t/\tau \approx 10^{-4.3} \text{ s}$$

or in $t = 10^4$, down by $10^{-4.3}$

at $t = 100^4$, down by $10^{-4.3}$

list

viscous

most
not
reasonable
see.

Ex 6.8

$$m = 2g = .002 \text{ kg}$$

in oil and

reaches $v_T = 5 \text{ cm/s}$

determine τ and t such that $v = .9v_T$?

$$v_T = \frac{g}{D} = g\tau \text{ and so } \tau = \frac{v_T}{g}$$

$$= \frac{5 \text{ cm/s}}{980 \text{ cm/s}^2}$$

$$\approx .005 \text{ s}$$

$$\text{Ans } .0051$$

$$v = v_T [1 - e^{-t/\tau}]$$

solve for t

$$\frac{v}{v_T} - 1 = -e^{-t/\tau}$$

$$e^{-t/\tau} = 1 - \frac{v}{v_T}$$

$$t/\tau = -\ln(1 - \frac{v}{v_T}) = -\ln(1 - .9) = -\ln(.1) \approx 2.3026$$



$$t = \tau \ln 10$$

$$\approx \tau * 2.3$$

$$= 11.5 \times 10^{-3} s$$

$$\approx 10^{-2} s$$

$$\text{Ans } 11.7 ms$$

$$= 10 ms$$

Actually Hoag
follows from
uncall eqn.
on way - 403, Bachelon
539

Case 2

For objects moving

Blunt objects
and - ball
not Tavelin
- air becomes
turbulent around
the object, -- breaks
up into
trailing
swirls

at higher speeds in fluids
- reaching higher V_T like air

in fact the resistive force
is more like a quadratic
in speed.

$$D = \frac{b}{m}$$

$$\propto \frac{V}{m} = \frac{A}{\rho A_{\text{rel}}}$$

for objects
of similar
shape L_{th}
resistive
force decreases
as L_{th}
increases

$$F_R = b V^2$$

$$b V^2 \approx \frac{1}{2} C_D \rho A V^2$$

drag coefficient
property of medium

cross sectional
projected area of object
perpendicular to motion

$$M \frac{L}{T^2} = [D] \frac{M}{L^3} L^2 \frac{L^2}{T^2}$$

$$= [D] M L / T^2$$

So D is dimensionless
HRN give
 D typical
values
of .4 to 1
for air

density of fluid
e.g. Air

6-52] This is just the magnitude
— the force opposes the direction
of motion

Now again we just consider
the illustrative case of sinking ^{starting}
(neglecting the buoyancy force) ^{below} _{next}

$$ma = F_{\text{net}}$$

$$\therefore ma = mg - bv^2$$

$$a + \frac{b}{m} v^2 = g$$

$$\frac{dv}{dt} + D v^2 = g$$

where $D = \frac{b}{m}$ again.

but here

$$[D v^2] = \frac{L/T}{T}$$

$$[D] \left(\frac{L}{T}\right)^2 = \frac{L/T}{T}$$

$$[D] = \frac{1}{L}$$

except for v^2 instead of v
this D is like the last one.

But that v^2 makes
a huge difference.

6-53

This is a non-linear DE
~~but~~ because the solution or
some derivative of it enters
non-linearly.

Most non-linear DEs do NOT
have analytic solutions

↳ i.e., exact single formula
solutions.

They can be solved with certain
approximations or numerically
but there is always some error
although it can often be made
as minute as you like for practical
purposes.

Quit

I've actually worked out an
approximate interpolation formula
for v which I'd guess is pretty
accurate, but it's too much bother
to test ~~and so~~ right now.

(See my own notes on SJ-I-18)

6-54) But we can still extract some partial information.

Since the object starts from rest $v = 0$ initially and we again expect

$$\frac{dv}{dt} \cong g \text{ at early times}$$

on $v \cong gt$

$$a = g - D(v_T + v) \\ g = -D(2v_T + v) + \frac{g}{3}$$

As v grows the resistive force grows and qualitatively we ^{guess} expect the same asymptotic approach to a terminal velocity v_T

It can be shown that this is true, but I'll forbear

$$\frac{dv}{dt} = 0$$

$$D v_T^2 = g$$

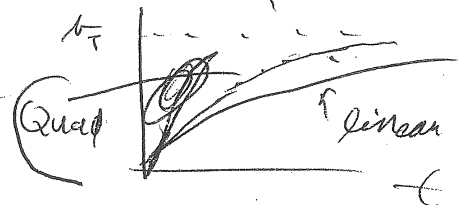
$$v_T = \sqrt{\frac{g}{D}}$$

or $0 \leq v$

$$a = g - Dv^2 \\ v \leq v_T \\ a > 0 \\ g - v > v_T \\ a < 0 \\ v = \sqrt{\frac{g}{D} - \frac{a}{D}} \\ = v_T \sqrt{1 - \frac{a}{g}}$$

When would we guess a transition between

the linear regime and asymptotic regime.



Well the linear regime
must be over when when
linear growth would take
the velocity to N_T

$$\therefore N_T = g t_{\text{characteristic}}$$

$$t_{ch} = \frac{N_T}{g} \approx \frac{N_T}{\frac{10^4}{s^2}} \left\{ \frac{L/T^2}{L/T^2} \right\} = T$$

$$\gamma_{ch} = \frac{1}{2} g t^2 = \frac{1}{2} g \frac{N_T^2}{g^2} = \frac{1}{2} \frac{N_T^2}{g}$$

~~Orbit?~~ or leave as question.

numerical solution of a DE. On another way - the One Step

$$a \approx \frac{N_T - 0}{t_{ch_2}} = g - D \left(\frac{N_T}{2} \right)^2$$

The same
number to
~~and~~ roughly
speaking.

$$t_{ch_2} = \frac{N_T}{g - D \left(\frac{N_T}{2} \right)^2}$$

$$= \frac{N_T}{g - \frac{g}{N_T^2} \left(\frac{N_T}{2} \right)^2}$$

$$= \frac{t_{ch}}{1 - \frac{1}{4}} = \frac{4}{3} t_{ch}$$

Terminal velocities in Air

6-56

typical values

HRW-105

ball from vest, 11 not from high speed

Object

V_T (m/s)

t_{oh} (s)

95% y (m)

y_{ch} (m)
 $= \frac{1}{2} g t^2$

Shot (from shot gun)	145	14.5	2508	
Shotgun (typical)	60 = 216 km/h = 140 mi/h	6	430	180
baseball	42	4.2	210	
Tennis ball	31	3.1	115	
pingpong ball	9	.9	10	
raindrop	7	.7	6	2.5
parachutist	5	.5	3	

cat tucked with feet extended to soften

27 = 97 km/h

3

36

cat spread

19 = 68 km/h

2

18

As the result of extensive (not to mention ballistic) experiments on cats

HRW-104

HRW
says
 $y_{tot} \approx 1.8m$
= 6.3

— when first thrown off a tall building — actually cats usually jump (they're just so smart you know)

right themselves
cat
Righting
Reflex.

— they first ~~tuck up~~ & extend feet down to cushion landing
→ they notice the acceleration
→ must be from the ~~drag~~ ^{retardation} force which is a contact force

then after they reach

Wick claims it's a natural reflex if they have time which makes more sense to me - it's a righting reflex.

$$v_{T \text{ ~~tucked~~ pounce}} = 27 \text{ m/s} \quad \text{above } \sim 18 \text{ m} \text{ or } 37 \text{ m?}$$

they feel safer and stretch out and ~~reduces~~ reduces v_T to $v_{T \text{ stretched out}} = 18 \text{ m/s}$ which is much smaller than human 60 m/s .

must be the cross-section.

$$\propto \frac{A}{\cancel{m}} = \frac{A}{\rho V} = \frac{A}{\rho A l_{+h}} = \frac{1}{\rho l_{+h}}$$

a Cat is $\sim \frac{1}{3}$ of a human in length

Cat l_{+h} maybe a bit smaller than human.

— all that ~~other~~ fur and skin folds may make a difference.

6-58

— no cat decelerator
to $V_T = 20 \text{ m/s}$

— as ground approach,
it sees that and and pulls
legs in for a softish landing
(to pounce mode)

It doesn't always work,
but apparently ~90% of cats
who fall to 2-32 stories
survive $\rightarrow$ their injuries are
less if they fall more than
6 stories $\sim$ 18 m (WIK)

$\rightarrow$ of course this statistic may
not count many who
simply died and no one
bothered to take them to
vet — ^{let's} put buried fluffy in
an old shoe box?"