

Ch 32 Inductance

32-1

Well we've actually already in Ch. 31 been dealing with inductance.

Faraday's law (and the universal flux rule) tell us changing magnetic fields create induced emfs, which if there is a conductor around create induced currents and induced B-fields.

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In this chapter
we focus on changing
currents causing
changing B-fields
causing induction.

§ 32.1 Self Inductance & Inductance

$$\mathcal{E} = - \frac{d\Phi_B}{dt}$$

$$\mathcal{E} \propto \frac{dB}{dt} \propto \frac{dI}{dt}$$

So
Area or
angle of
the flux
surface isn't

for certain setups where
the path of the emf is fixed
and a current gives rise
to the B

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which is pretty
much always true
in circuit setup

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(not in ^{electric motors or generators or} free propagating
electromagnetic waves)

So in circuit setups

$$E \propto \frac{dI}{dt}$$

and we can write

$$E = -L \frac{dI}{dt}$$

For cases where the induced emf is in the ~~system~~ circuit that gave rise to it.

where L is called ~~the~~ inductance or self inductance

L is determined by the geometry of the system

or device

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(and any magnetic materials around, but we won't go into that much)

A device

designed

to have an inductance in an inductor

It independent of I and E ideally.

— but circuits will have ^{inevitable} ~~accidental~~ ^{self} inductances like it or not — usually those are pretty small.

The minus sign in

$$E = -L \frac{dI}{dt}$$

is conventional and tells us the induced emf opposes the ^{changes in} current.



~~We did an example of an~~

opposes changes in current.

maybe not for circuit cases

— One can use the convention to find the sense of the emf, but Lenz's law is easier

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Units of L

$$[L] = \left[\frac{\mathcal{E}}{\frac{dI}{dt}} \right] = \frac{V}{A/s^2}$$

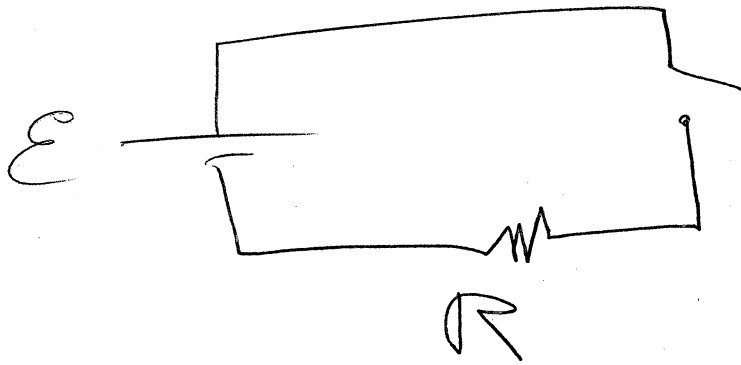
$$= \frac{J \cdot s^2}{C^2}$$

$$= \frac{J}{A^2}$$

$$\equiv 1 H$$

a henry for
Joseph Henry
who independently
discovered
Faraday's
law about
the same
time as Faraday.

Ex 2: Ineluctable Inductance



~~We've~~ When the circuit is closed we've ignored the rise phase of current from 0 to steady state

$$I = E/R$$

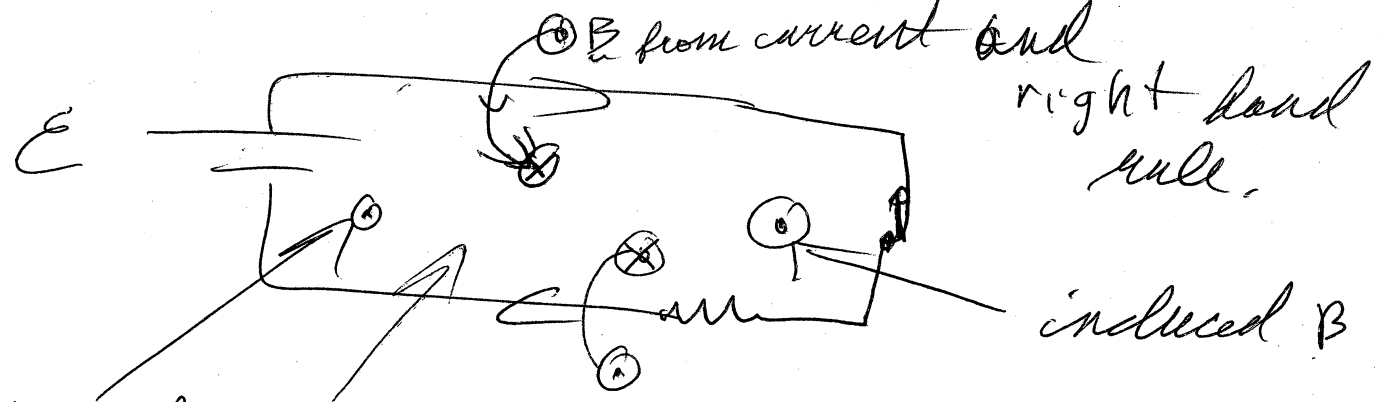
- For circuits without inductors, that phase is pretty ~~fast~~ short, but it isn't zero time:

a) because it does take a finite time for the static guide of electric fields to establish charge a steady state.

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b) Which is actually a subset of (a), self-inductance.

— as current flow



but as Φ_B in this loop grows

an induced $\mathcal{E}_{induced}$ is created by Faraday's law around the loop with the sense of opposing B 's grows

~~by~~ by created an induced B

$\mathcal{E}_{\text{induced}}$
opposed \mathcal{E} .

~~So really the ar~~

Say L_{circuit} is the inductance,

then ignoring other delay effects (which may or may not be valid since L is likely pretty tiny in this case) Kirchoff's voltage

law gives

$$\mathcal{E} - L \frac{dI}{dt} - IR = 0$$

$\mathcal{E}_{\text{induced}}$

going around the loop.

For such circuits L is

32-10) usually negligibly
small depending on
how accurate you are
being and we usually assume $L_{cor} = 0$

But an actual inductor
device ^{with} ~~with~~ a finite
 L will have an effect
as we'll see.

Ex Calculation of L
for an ideal solenoid

— we did this example before
and so this is a repetition

↳ an ideal solenoid — one that
can be made is infinite in length
even if it isn't.

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$$i. \quad \mathcal{E} = - \frac{d\Phi_B}{dt}$$

net emf

$$= N \mathcal{E}_{\text{turn}}$$

$$= - \frac{\mu_0 n^2 V}{l} \frac{dI}{dt}$$

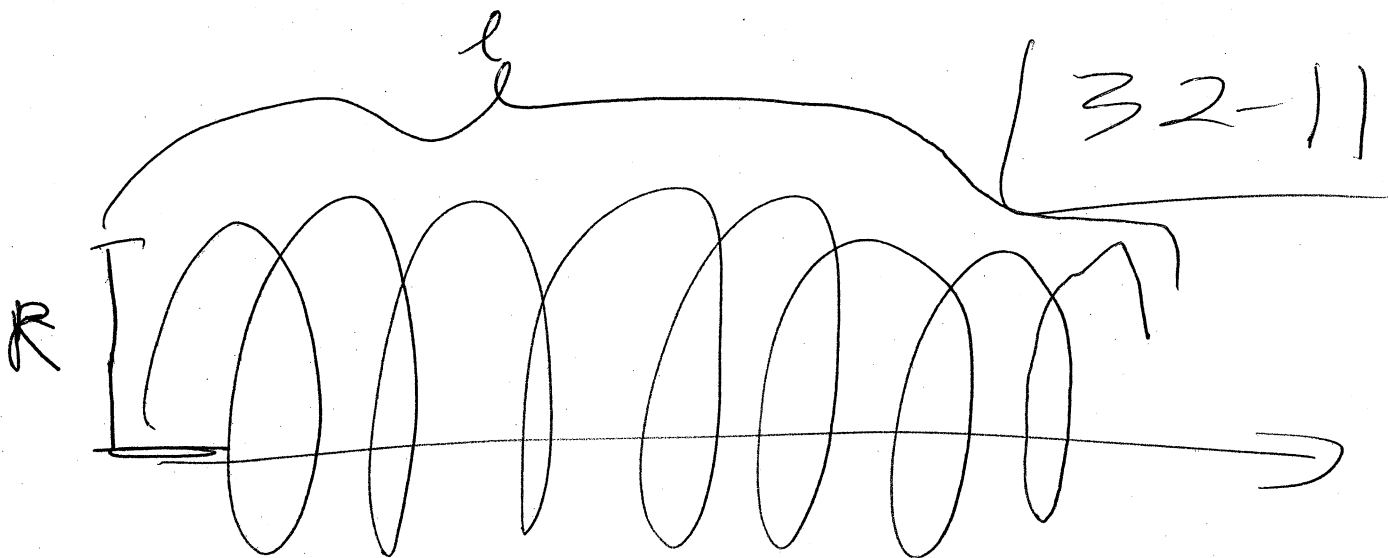
$$L = \mu_0 n^2 V_{\text{volume}}$$

$$L = \frac{\mu_0 N^2}{l} \quad (\text{ST-899 agree})$$

So the inductance depends on the geometry.

— filling the solenoid with a magnetic material would enhance L by a factor of μ_r (the relative permeability) (e.g.) soft iron
 (μ_r : inductance)

actually this depends on applied magnetic flux usually and simplicity is lost,



$$B = \begin{cases} \mu_0 n I & \text{inside} \\ 0 & \text{outside} \end{cases} \quad \left. \begin{array}{l} \text{from} \\ \text{Ampere's} \\ \text{Law.} \end{array} \right\}$$

So inside uniform in direction and magnitude

n is number of turns per unit length. $= N/l$ where N is the number of turns

$$\Phi_{\text{one turn}} = \pi R^2 B = \pi R^2 \mu_0 n I$$

~~$= \mu_0 n R^2 I$~~

$$\Phi_B = N \Phi_{\text{one turn}} \quad \text{---} \mu_0 n R^2 \frac{N^2}{l} I \text{---}$$

Total flux linked by solenoid.

$$= n l \pi R^2 \mu_0 n I$$

$$= \mu_0 n^2 I \text{ Volume} \quad \left(\begin{array}{l} \text{Volume} \\ = l \pi R^2 \end{array} \right)$$

but we won't worry 32-13
about such complications

Let's evaluate a fiducial
value for L

$$\mu_0 = 4\pi \times 10^{-7} \text{ we call}$$

$$R = 1 \text{ cm} = .01 \text{ m}$$

$$l = 1 \text{ m}$$

$$N = 1000$$

$$n = 10^3$$

$$V = \pi R^2 l \\ \approx 3 \cdot 10^{-4} \cdot 1 \\ = 3 \cdot 10^{-4}$$

$$L \approx \overset{\mu_0 N^2 n^2}{4\pi \times 10^{-7} \cdot 3 \cdot 10^{-4} \cdot 10^6}$$

$$= 40 \cdot 10^{-5}$$

$$= 4 \times 10^{-4} \text{ H}$$

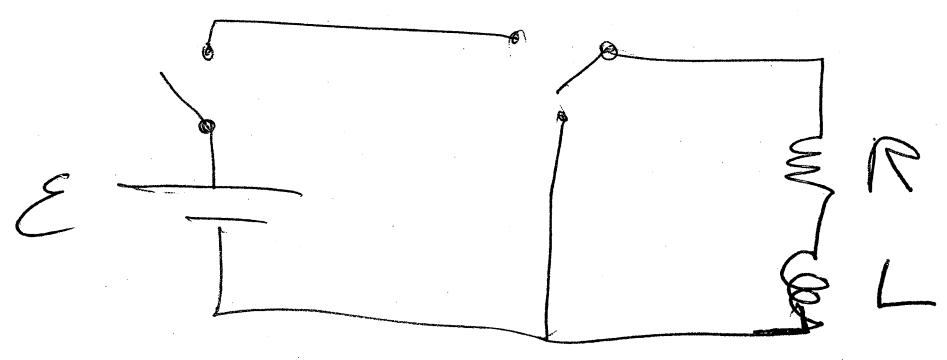
$$= .4 \text{ mH}$$

$$\text{Say } \frac{dI}{dt} = 1 \text{ A/s} \quad \text{,} \quad \mathcal{E}_{\text{ind}} = .4 \times 10^{-4} \text{ V} \\ = .4 \text{ mV}$$


32-14)

§ 32.2 RL circuits

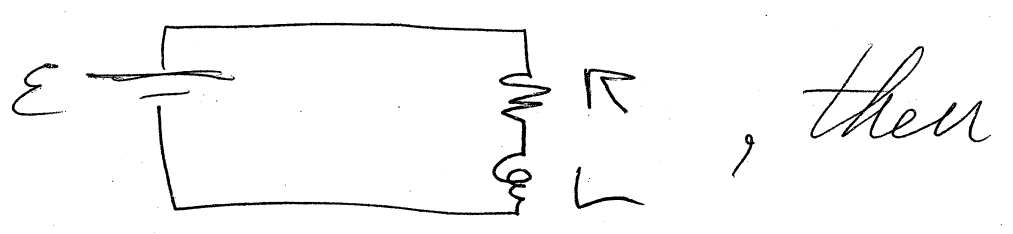
RL means they have a resistor and an inductor.



- we assume the wires are ideal - no resistance, no inductance.

inductor symbol 

if we close to get



Kirchhoff's
voltage law
gives

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$$\mathcal{E} - L \frac{dI}{dt} - IR = 0$$

Count
as a
drop in
direction
of current
flow
(come into
a wire if
 $\frac{dI}{dt} < 0$)

induced
emf
opposes
~~the applied~~
current the
applied emf tries to
establish.

This is a differential
equation (DE) not an algebraic one.

— actually a linear, 1st order,
homogeneous DE.

It can be solved—
but the techniques
are beyond our scope.

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So we'll just
write ~~down~~ the solution
and confirm it ~~later~~
below.

$$I = I_{\infty} (1 - e^{-t/\tau})$$

where $\tau = \frac{L}{R}$

is the e-folding time
or time constant

When a steady state
is reached $\frac{dI}{dt} = 0$

and so $\mathcal{E} - I_{\infty} R = 0$

then and $I_{\infty} = \frac{\mathcal{E}}{R}$

$$\frac{dI}{dt} = I_{\infty} \left(\frac{e^{-t/\tau}}{\tau} \right)$$

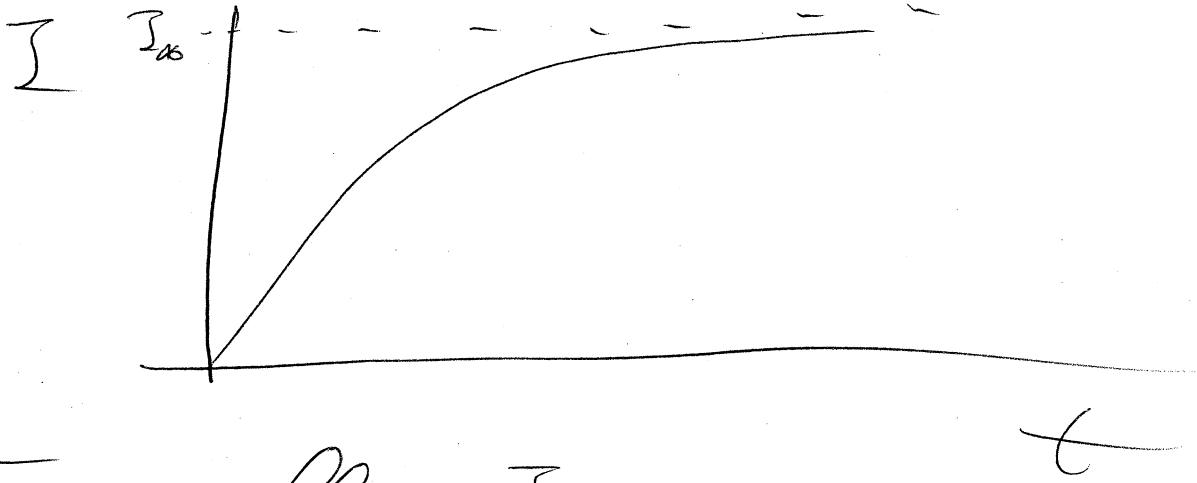
$$\mathcal{E} - L \frac{\mathcal{E}}{R} \frac{e^{-t/\tau}}{\tau} - R \frac{\mathcal{E}}{R} (1 - e^{-t/\tau}) = 0$$

$$\therefore 1 - e^{-t/\tau} - (1 - e^{-t/\tau}) = 0$$

and so we've
confirmed the solution.

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~~Formally~~



Formally I never
reaches I_{∞} .

But in any real circuit
there is uncertainty in current
measurements ΔI_{err}

and current fluctuations ΔI_H
(due all kinds of low level
things — thermal fluctuations,
stray E-fields (although
they may not penetrate the
conductors)
much.)

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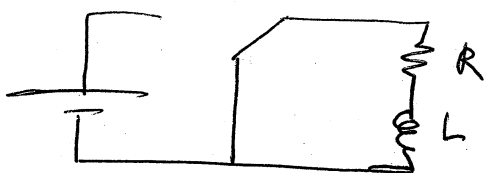
Once $|I - I_{\infty}| < \Delta I_{\text{err}}$ or ΔI_{fl}

then practically I has
reached I_{∞} .

^a This may happen within
a few folding times depending
on how precise one is
being.

The inductor slows the
rise of the current
to I_{∞} .

The other case of the
circuit is when one suddenly



Now $I_0 = I_{\infty}$

initial
current of the
new phase.

In this case Kirchhoff's
voltage law gives

$$-IR - L \frac{dI}{dt} = 0$$

A voltage potential drop

Now $\frac{dI}{dt} < 0$
a potential
rise that
tries to maintain
the current.
— the induced emf
opposes changes.

We know the final
state $I_{\infty} = 0$

→ when steady state is reached
 I_{∞} is constant, but then

$$I_{\infty} R = 0 \text{ for the Voltage law}$$

$$\therefore I_{\infty} = 0.$$

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We can guess

$$I = I_0 e^{-t/\tau}$$

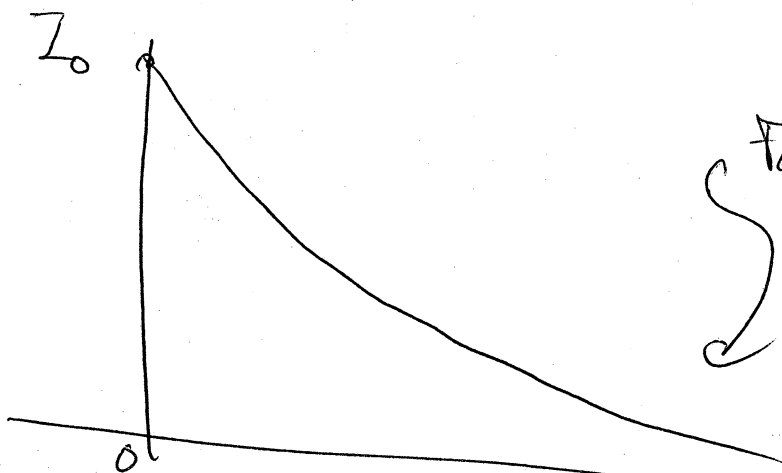
$$\therefore = I_0 e^{-t/\tau} R - L \left(-\frac{1}{\tau}\right) I_0 e^{-t/\tau} = 0$$

$$= R + R = 0$$

and so

$$I = I_0 e^{-t/\tau} \text{ is}$$

the relation
of the DE



Formally the current never goes to zero, but practically it does after a few τ (oldiy) times depending on what one's error & fluctuations

§ 32.3 Energy

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in a Magnetic Field

The power transferred in an inductor is

$$P = V_{\text{drop across}} I$$

at any instant.

$$\text{Now } V_{\text{drop across}} = \mathcal{E}_{\text{induced}}$$

from the electrostatic force pushing the current along

from the induced electric field preventing acceleration of current.

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$$\mathcal{E} = L \frac{dI}{dt}$$

$$P = L \frac{dI}{dt} I$$

Assuming

$$I > 0$$

if I is increasing
the power is going
out of the circuit
somewhere.

if I is decreasing
power is coming from
somewhere into the circuit

~~Energy
stored
released~~

$$W = \int \frac{dI}{dt} I dt$$

$$= L \int_0^I I' dI' = \frac{1}{2} LI^2$$

$$U = E_{\text{stored}} = \frac{1}{2} L I^2 \quad \left| \begin{array}{l} 32-23 \end{array} \right.$$

if you create a current starting from $I = 0$ and raising it to I .

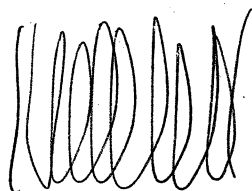
We don't call this stored energy potential energy — the term doesn't seem to be a good fit. } I_{sm} a fit.

But after our experience with electric fields, it should come as no surprise that the energy is stored in the magnetic field created by the current.

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Just as with \mathbb{F} -field case, we can't ~~prove~~ this — beyond our scope, but we can elucidate it.

Let's approximate an inductor as an ideal solenoid.


$$B = \begin{cases} \mu_0 n I & \text{inside} \\ 0 & \text{outside} \end{cases}$$

recall

n is the number of turns per unit length.

Now recall $V_{\text{self, solenoid}} = \mu_0 \frac{N^2}{L} \frac{A I^2}{2}$

$$L \approx \mu_0 n^2 V_{\text{vol}}$$

(res-899)

$$U = \frac{1}{2} L I^2$$

$$= \frac{1}{2} \mu_0 \cancel{N^2 A} \frac{B^2}{\mu_0^2 n^2}$$

$$= \cancel{\frac{N^2 A}{2 \mu_0}} \frac{B^2}{2 \mu_0}$$

$$= \cancel{V} \frac{B^2}{2 \mu_0}$$

Volume of solenoid.

∴ one might guess

$$u = \frac{U}{V} = \frac{B^2}{2 \mu_0}$$

And we are right. This is the general result — but we can't prove it.

is the energy density of magnetic field. (for vacuum)

Recall $u = \frac{1}{2} \epsilon_0 E^2$

is the energy density of the electric field.

which are nearly identical speaking

32-16)

As we'll see in Ch 34

$$c = \frac{1}{\sqrt{\mu_0 \epsilon_0}}$$

and

$$\text{so } \frac{u_B}{u_E} = \frac{\frac{B^2}{2\mu_0}}{\frac{1}{2}\epsilon_0 E^2}$$

$$= \frac{1}{(\mu_0 \epsilon_0)} \frac{B^2}{E^2}$$

$$= c^2 \frac{B^2}{E^2}$$

which ~~may~~ probably means something important, but it eludes me at the moment.

$E \times$ for Fiducial cases

$$u_E = \frac{1}{2} \epsilon_0 E^2$$

$$u_B = \frac{B^2}{2\mu_0}$$

$$\text{So } E = 1 \text{ V/m}$$

$$\epsilon_0 = 8.854 \times 10^{-12}$$

$$u_E \approx 4.4 \times 10^{-12} \text{ J/m}^3$$

$$B = 1 \text{ T}$$

$$\mu_0 = 4\pi \times 10^{-7}$$

$$u_B = \frac{1}{8\pi} \times 10^7 \\ \approx 4 \times 10^5 \text{ J/m}^3$$

which numbers are actually consistent with what we'd ordinarily think

$I V_m$ is not a very large E -field

but $I I$ is a pretty big B -field.

Ex 32.3

What happens to the energy of an inductor in the fiducial decaying current case



at $t = 0$

$$I = I_0$$

We know that

$$I = I_0 e^{-t/\tau}$$

32-28

where $\tau = \frac{L}{R}$

$$U = \frac{1}{2} L I^2$$

$$= \frac{1}{2} L I_0^2 e^{-2t/\tau}$$

~~the~~ show declining

energy. $P_{out} = \frac{dU}{dt} = - R I_0^2 e^{-2t/\tau}$

In the resistor the power is less than zero and so a loss

$$P = V I = \cancel{P} = I^2 R$$

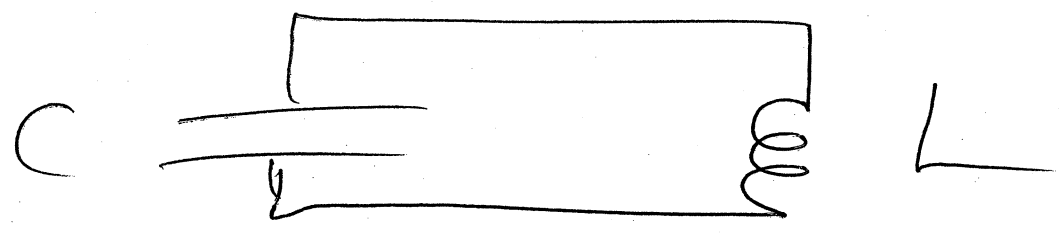
which is going into waste heat (which is something we thermodynamics).

$$P = R I_0^2 e^{-2t/\tau}$$

out put of resistor to waste heat.

So the ~~power~~ ^{energy} ~~from~~ stored in the magnetic field is converted to waste heat in the resistor.

§ 3 2.5 Oscillation in an LC circuit.



a capacitor inductor circuit
— so LC circuit.

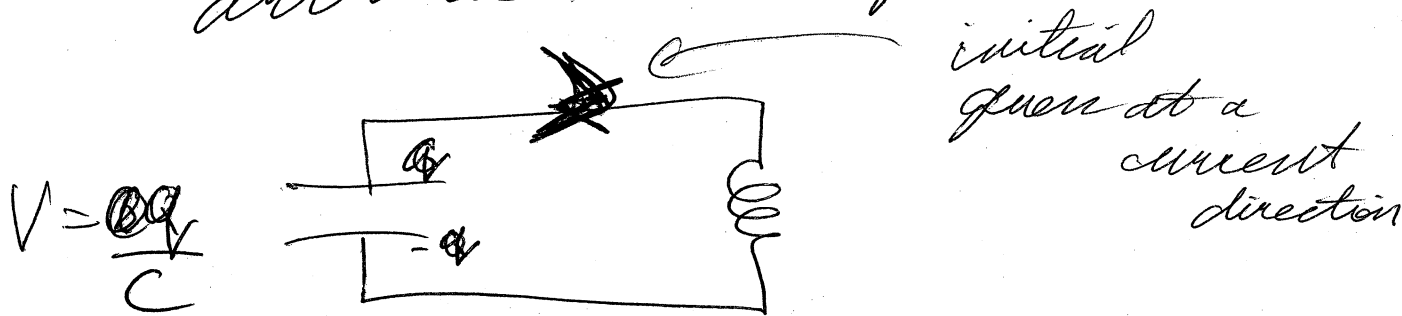
— As we see it here, it's a bit isolated and abstract
— but LC circuits are included in ~~Q~~ electronic oscillators to create sinusoidal electrical signals

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and low filters
and tuners,

but it goes beyond
our scope to go into
the practicalities (right now. We
do a bit
in Ch. 33)
— we just look at
the essence.

Apply Kirchoff voltage law
around the loop.



$$Cq - L \frac{dI}{dt} = 0$$

rise
as we
drawn it

a drop

for our chosen direction
assuming $\frac{dI}{dt} > 0$

This
assumption
does
work
out.

Now $I = - \frac{dq}{dt}$

— the current we count as positive comes at the expense of the charge on the capacitor.

$$\frac{q}{C} + L \frac{d^2 q}{dt^2} = 0$$

$$\frac{d^2 q}{dt^2} = - \frac{1}{LC} q$$

define $\omega = \sqrt{\frac{1}{LC}}$

$$\frac{d^2 q}{dt^2} = -\omega^2 q$$

$$\left\{ \begin{aligned} [L] &= \frac{V \cdot s}{A} \\ [C] &= \frac{C}{V} \\ \left[\frac{1}{LC} \right] &= \frac{(A/s)^2}{V \cdot C} \\ &= \frac{1}{s^2} \\ &= \frac{1}{s} \end{aligned} \right.$$

which is the simple harmonic oscillator differential equation

$$\frac{d^2 x}{dt^2} = -\omega^2 x \quad \square$$

also

$$\frac{d^2 \theta}{dt^2} = -\omega_0^2 \theta$$

$\nearrow P$
for oscillating electric dipole
 $\rightarrow B$

32-32

The systems systems are physically different, but they have the same mathematical description

— decades of experience tells me the general ~~rotator~~ solution is

$$q = A \cos \omega t + B \sin \omega t$$

$$\frac{d^2 q}{dt^2} = -A \omega^2 \cos \omega t - B \omega^2 \sin \omega t = -\omega^2 q$$

and that confirms the solution.

~~Say~~ A and B are constants set by initial conditions.
Nothing in the physics of the

32-34

So increasing either
 L or C increases
the period and decreases
the oscillation frequency.

Example

Say at time zero

$$Q = Q_0$$

and we've just
~~hooked~~ connected
the capacitor to a
zero current inductor.

$$Q = Q_0 \cos(\omega t) + B \sin \omega t$$

The time zero condition gives $A = Q_0$

$$I = -\frac{dQ}{dt} = + Q_0 \omega \sin \omega t - B \omega \cos \omega t$$

system tells us what they are. [32-33]

— This is often the case in physical system — well always except maybe the universe as a whole — physical tells us something, but to know everything we need the initial conditions or the boundary conditions.

Example The sinusoidal functions are periodic.
Every time t increases by Δt such that $\omega \Delta t = 2\pi$, the q value repeats.

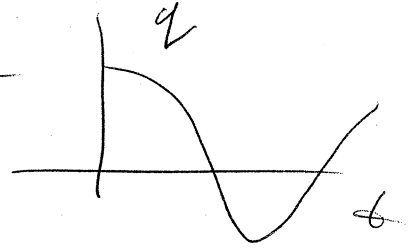
$$P = \frac{2\pi}{\omega} = 2\pi \sqrt{LC} \text{ is the period.}$$
$$= 2\pi \sqrt{LC}$$

Since $I = 0$ at time zero

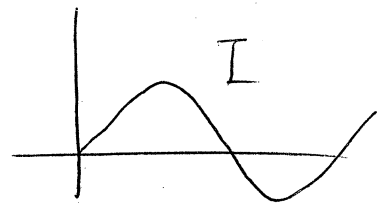
32-35

$$B = 0$$

$$q = q_0 \cos \omega t$$



$$I = q_0 \omega \sin \omega t$$



$$U_{\text{cap}} = \frac{q^2}{2C}$$
$$= \frac{q_0^2}{2C} \cos^2 \omega t$$

$$U_{\text{ind}} = \frac{1}{2} L I^2$$

$$= \frac{1}{2} L q_0^2 \omega^2 \sin^2 \omega t = \frac{1}{2} \frac{1}{C} q_0^2 \sin^2 \omega t$$

recall

$$U_{\text{cap}} + U_{\text{ind}} = \frac{1}{2} \frac{q_0^2}{C} (\cos^2 \omega t + \sin^2 \omega t)$$
$$= \frac{1}{2} \frac{q_0^2}{C}$$

— a constant.

— the energy oscillates back and forth between capacitor

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and inductor energy
but is overall conserved.

There is no way in the
system for energy to come
from or go to.

— In LRC circuit,
energy can be dissipated
in the resistor and
~~the~~ initial energy decays.

Example periods

$$P = \begin{cases} 2\pi\sqrt{LC} \\ \underbrace{2\pi}_{6.28} \text{ s for } L=1\text{H}, C=1\text{F} \end{cases}$$

$$2\pi \sqrt{10^{-3} \cdot 10^{-6}} \left\{ \begin{array}{l} L = 1 \text{ mH} \\ F = 1 \mu\text{F} \end{array} \right.$$

$$\cong 20 \times 10^{-5}$$

$$= 2 \times 10^{-4} \text{ s}$$

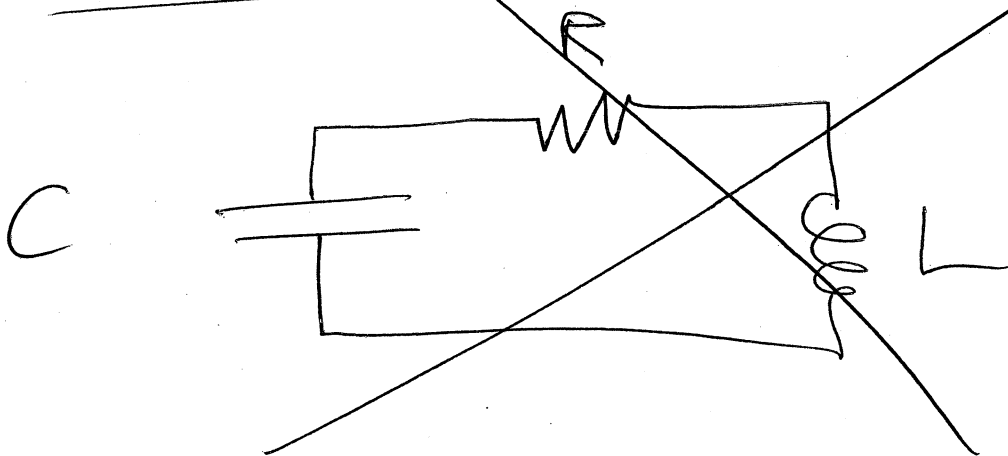
Now $f = \frac{1}{P} = \frac{1}{2\pi \sqrt{LC}}$

is frequency in Hertz.

$$\therefore f = \frac{1}{2 \times 10^{-4} \text{ s}} = .5 \times 10^4 \text{ Hz}$$

$$= 5000 \text{ Hz}$$

~~§ 32.6 RLC circuit (omit?)~~



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Applying Kirchhoff's
voltage law

$$\frac{q}{C} - IR - L \frac{dI}{dt} = 0$$

or rise two drops.

$$L \frac{d^2q}{dt^2} + \frac{dq}{dt} R + \frac{q}{C} = 0$$

or differentiating once
and re-arranging $I = -\frac{dq}{dt}$

$$L \frac{d^2I}{dt^2} + \frac{dI}{dt} R + \frac{I}{C} = 0$$

If $C \rightarrow \infty$, like memory
the capacitor and replacing
with a connection
and we have an RL
circuit

§ 32.6 RLC circuit

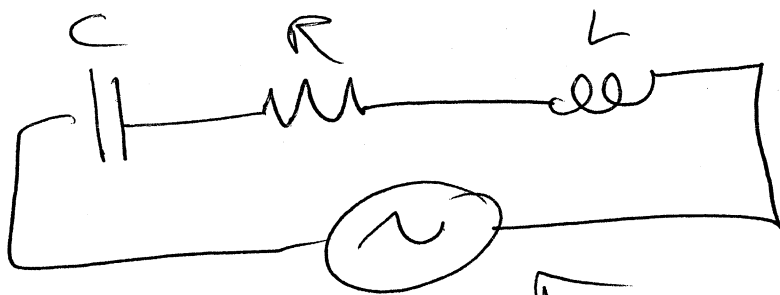
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RLC circuits contain resistor, inductor, capacitor.

The bare bones one has just those



One can add an AC emf



↑
symbol

(SI-932)

↑
This is an interesting case because multiple AC frequencies

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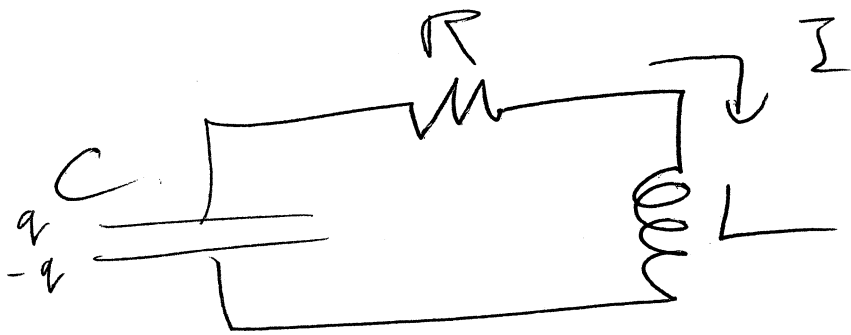
can be input to RLC circuit at one time and RLC (usually the C) can be adjusted to respond strongly only to a narrow range of AC frequencies.

This allows "tuning" as for a radio (ST-939)

But here we'll only consider the barebones case.

To understand 32-4

More complex cases
 (which I don't think
 we'll do in this course),
 one has to understand
 the barebones RLC circuit



Apply Kirchhoff voltage law

Going around the loop counterclockwise	$\frac{q}{C}$ <hr style="width: 50%; margin: 5px auto;"/> a rise for $q > 0$ - drop for $q < 0$	$- IR$ <hr style="width: 50%; margin: 5px auto;"/> a drop for $I > 0$ rise for $I < 0$	$- L \frac{dI}{dt} = 0$ <hr style="width: 50%; margin: 5px auto;"/> a drop for $\frac{dI}{dt} > 0$ rise for $\frac{dI}{dt} < 0$
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$$\text{Now } -\frac{dq}{dt} = I$$

If q is decreasing, ^{of the top plate} there is a positive current

and if q is increasing on the top plate, there is a negative current.

So all our conventions ~~are~~ are consistent.

$$-\frac{d^2q}{dt^2} = \frac{dI}{dt}$$

$$\therefore \frac{q}{C} + q'R + Lq'' = 0$$

or in conventional form

32-44)

which is "always" true
for the context ~~is~~ ideally

by ~~from~~ physical law

and partially by initial
or boundary conditions.

How do we get the solutions?

We guess a trial solution

based on experience

and find out what

constraints the D.E. puts
on the guessed constants.

But before we do that

one can say the above

D.E. is exactly analogous

$$Lq'' + q'R + \frac{q}{C} = 0 \quad \left| \begin{array}{l} 32-43 \\ \hline \end{array} \right.$$

This is a linear 2nd order differential equation (DE) for q .

Math guarantees two independent solutions

— i.e., one solution can't be made out of the other.

— One also gets two constants

of integration set by

initial conditions

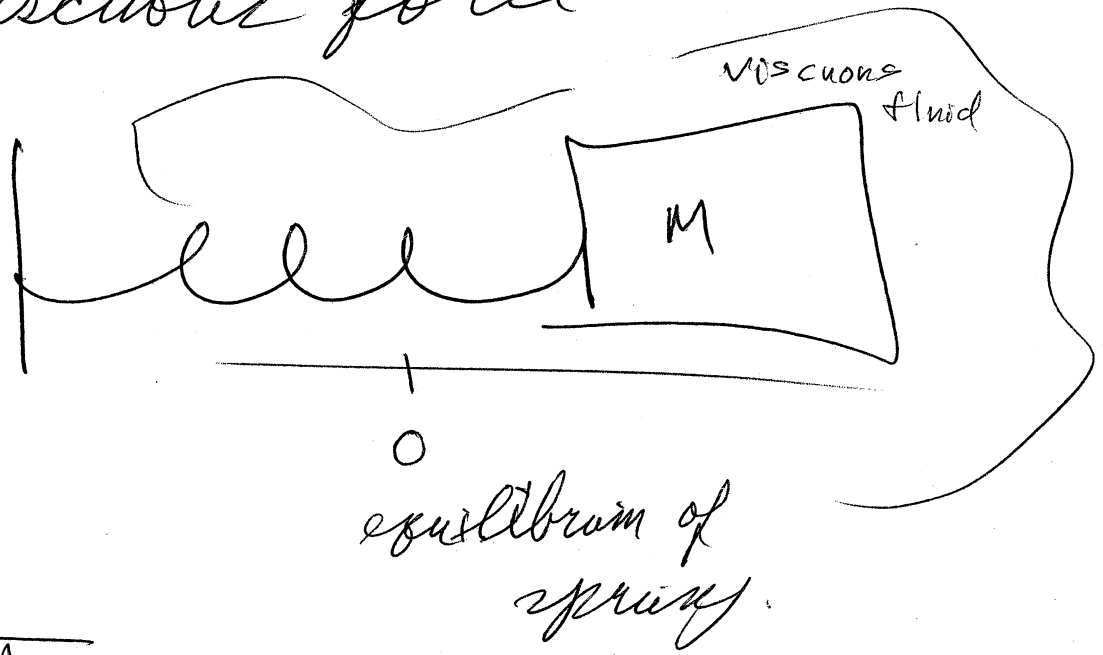
$$\left. \begin{array}{l} \text{To be definite} \\ q = q_0 \text{ at } t = 0 \\ i_0 = -\frac{dq}{dt} = 0 \text{ at } t = 0 \end{array} \right\}$$

→ This is frequently how things go in physics. A solution is partially determined

~~Part of a solution is determined~~

to a problem in ~~GM~~ mechanics.

↳ the damped harmonic oscillator problem where the damping force is a linear viscous force.



$$\underline{F}_{net} = ma$$

$$m \frac{d^2 x}{dt^2} = -kx - b \frac{dx}{dt}$$

linear restoring force or Hooke's law force

a linear viscous force that always opposes the direction of motion.

32-46)

Comparing the two DE's

$L \longrightarrow m$

acts like
~~the~~ inertia
and tries to
prevent "acceleration"

$\frac{1}{C} \longrightarrow k$

acts like
a force constant

$R \longrightarrow b$

acts like
a coefficient
ofth viscous force.
~~drag~~

— the mechanical motion could
be an oscillation from

a displacement

32-47

↳ but $b \neq 0$ would
cause it to be damped
out.

Similarly for our DE

q will turn out to
oscillate for certain
conditions, but for $R \neq 0$

the oscillation must come
to rest⁴ with $\dot{q} = 0, I = 0$
— It must damp out.

Solution (we go a bit beyond
text)

Consider the trial solution

$$q = q_0 e^{\alpha t}$$

32-4d)

where q_0 and α are undetermined constants.

Substitute into our DE and we get.

$$L\alpha^2 + \alpha R + \frac{1}{C} = 0$$

(cancelling out $q_0 e^{\alpha t}$)

Just an algebraic quadratic equation with solution

$$\alpha_{\pm} = \frac{-R \pm \sqrt{\left(\frac{R}{2L}\right)^2 - \frac{1}{LC}}}{2L}$$

from
$$\frac{-R \pm \sqrt{R^2 - 4LC}}{2L}$$

The general solution (32-48)
 with two undetermined constants
 is

$$q = A e^{\alpha_+ t} + B e^{\alpha_- t}$$

Actually it's helpful to
 look at the exponential
 constants α_{\pm} in terms of
 a time scale for decay.

$$\tau = -\frac{1}{\alpha_{\pm}} = \frac{1}{\frac{R}{2L} \pm \sqrt{\left(\frac{R}{2L}\right)^2 - \frac{1}{LC}}}$$

$$= \frac{2L/R}{1 \mp \sqrt{1 - \left(\frac{2\sqrt{L/C}}{R}\right)^2}}$$

$$\frac{2L}{R}$$

for $R < R_{crit} = 2\sqrt{L/C}$
 where as we'll show there
 is an oscillation and the
 complex τ can be interpreted
 as giving a complex
 oscillation

32-40c

$$\frac{2L}{R}$$

for $R = R_{crit} = 2\sqrt{\frac{L}{C}}$

or $\zeta = \frac{2L}{R} = \sqrt{LC}$

$$L/R$$

for $R \gg R_{crit}$

lower case relation

$$2L/R$$

$$1 - \left(1 - \frac{1}{2} \frac{4L/C}{R^2}\right)$$

for $R \gg R_{crit}$
upper case relation

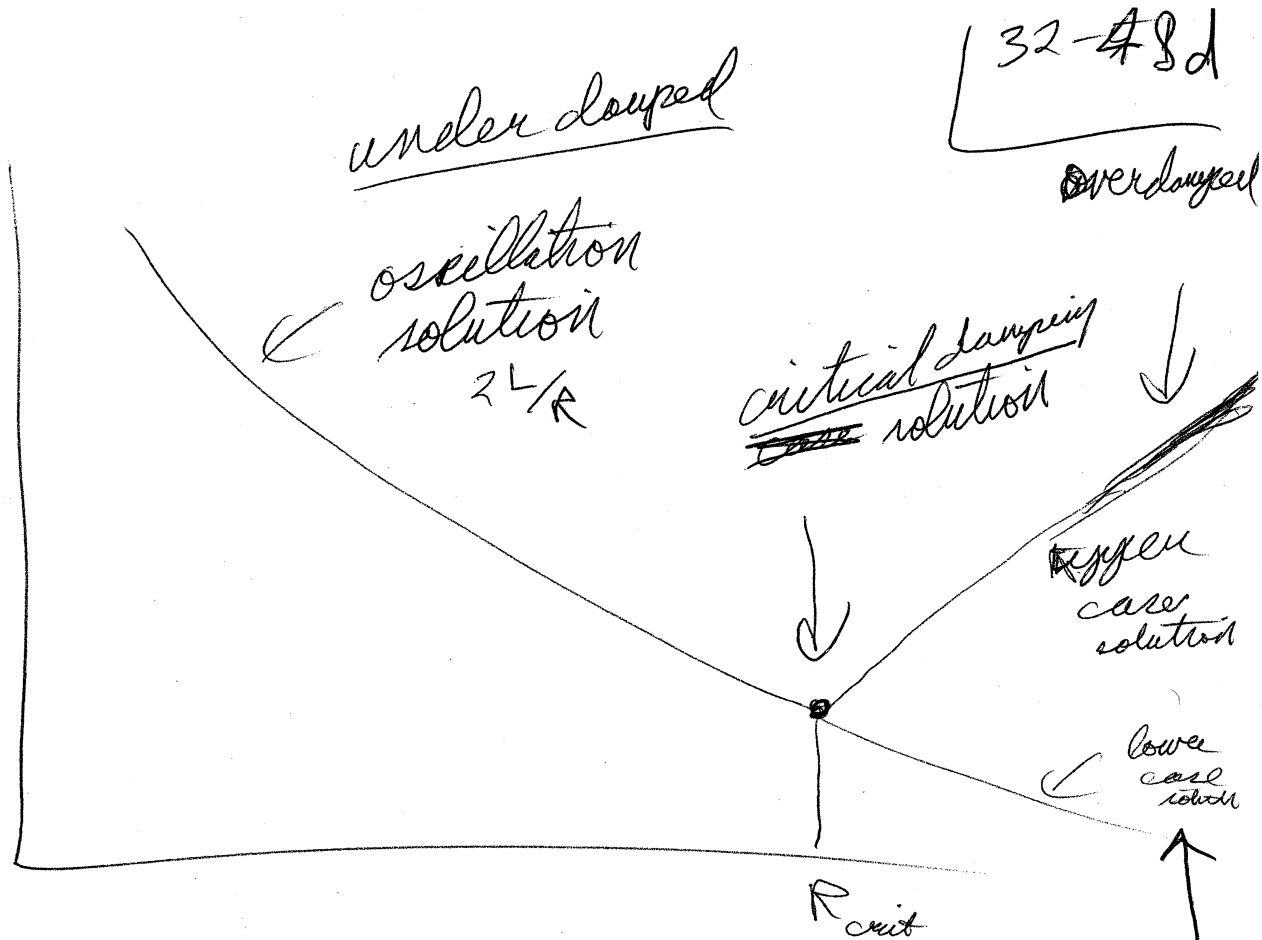
$$= RC \rightarrow L/R$$

for $R \gg R_{crit}$

Unless the coefficient of the relation is exactly zero.

and is the dominant long time scale for decay.

17



The critical damping case gives ζ minimum (not country)

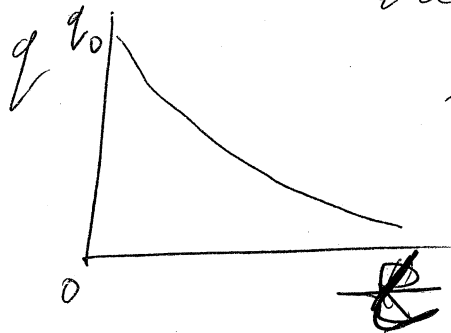
— this can be proven mathematically but I leave that to optional notes.
(that the R_{crit} gives ζ_{min})

ζ_{min} gives the fastest decay as long as the upper case overdamped solution is not set to zero.

32-48e

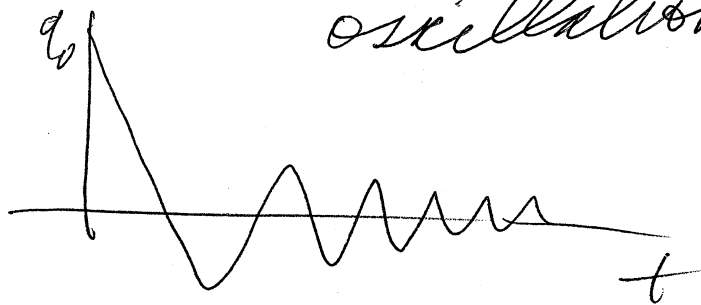
Overdamping is the $R > R_{crit}$
~~molasses~~
"molasses" solution

— the system can't come to equilibrium quickly because the resistance slows everything down.



Underdamped $R < R_{crit}$

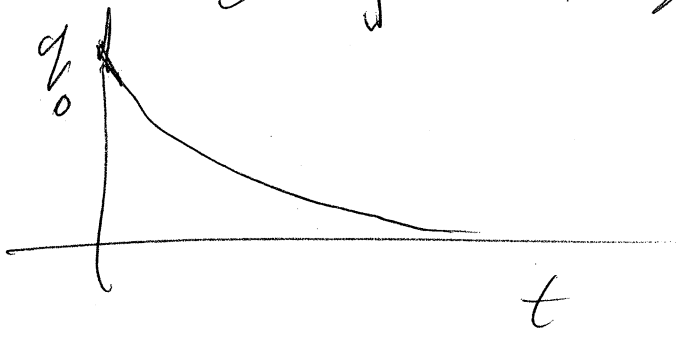
— here there is an overshoot because resistance is so small and oscillation



Critically damped

$$R = R_{crit}$$

is "just right" as



Goldilocks
would
say for
~~fastest~~
fastest
evolution
to $q = 0$.

Of course formally
 $q = 0$ is only
reached at $t = \infty$
in all cases,
but critical damping
gives the fastest approach
and so the fastest in
practical effect.

32-48g

The discriminant

32-49

$$d = \left\{ \left(\frac{R}{2L} \right)^2 - \frac{1}{LC} \right. \text{ in general}$$

$$> 0$$

then there is just a decaying solution.

- overdamped case

$$= 0$$

critically damped case

(For fixed L & C about the fastest case for either the motion.)

$$< 0$$

- complex solutions but the real parts are also solutions and these give oscillatory solutions

- underdamped case

32-50)

a) Overdamped $\left(\frac{R}{2L}\right)^2 - \frac{1}{LC} > 0$
or $R > R_{crit}$

$$q = q_+ e^{\alpha_+ t} + q_- e^{\alpha_- t}$$

$$\alpha_{\pm} = -\frac{R}{2L} \pm \sqrt{\left(\frac{R}{2L}\right)^2 - \frac{1}{LC}}$$

recall

always $< \left(\frac{R}{2L}\right)$

and so $\alpha_{\pm} < 0$

and both solutions are decaying exponentials.

~~0~~₊

$$-\alpha_+ < -\alpha_-$$

$$-\frac{1}{\alpha_+} > -\frac{1}{\alpha_-}$$

and so the α_+ case
is the more slowly declining

solution and
must dominate at
late times.

If we take initial conditions

$$\cancel{q_0 = 0} \quad q_0 = q_+ + q_-$$

$$\text{and } 0 = \dot{q}_0 = -\left. \frac{dq}{dt} \right|_0 \\ = q_+ \alpha_+ + q_- \alpha_-$$

then we can solve for q_+ and q_-

For the record

$$q_- = q_0 - q_+$$

$$\therefore 0 = q_+ \alpha_+ + (q_0 - q_+) \alpha_- \\ = q_+ (\alpha_+ - \alpha_-) + q_0 \alpha_-$$

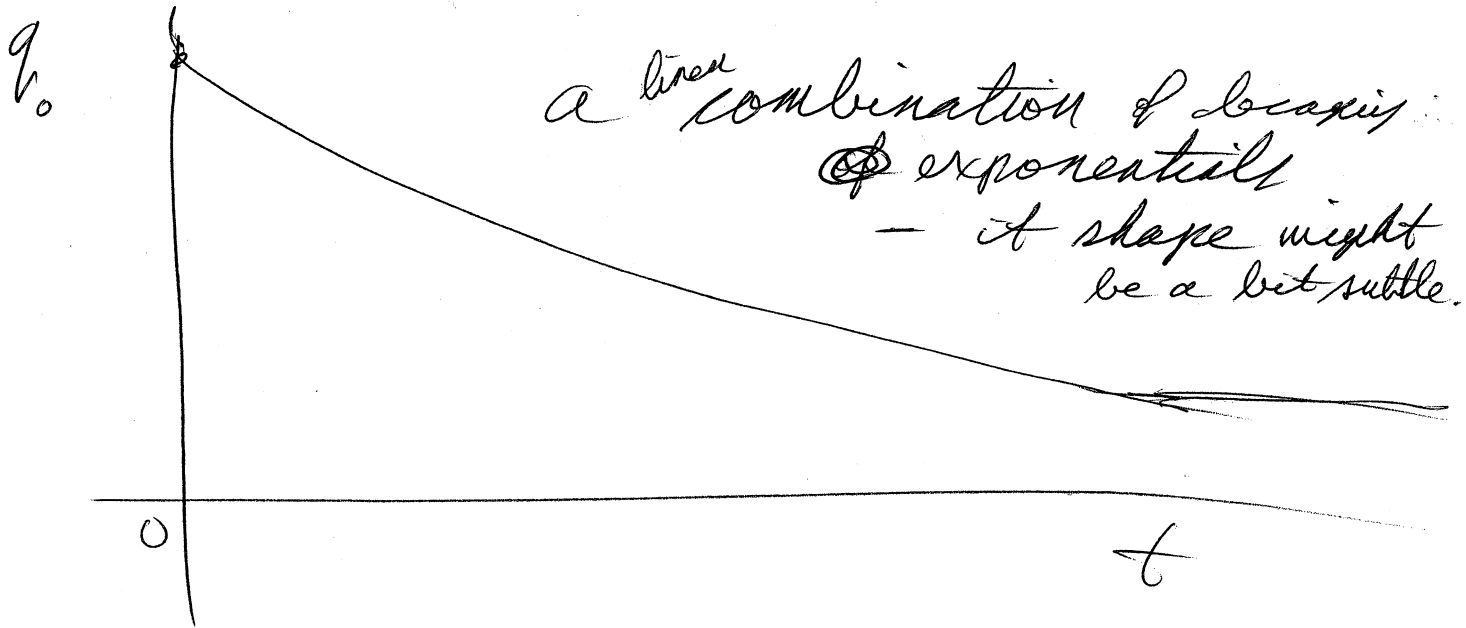
$$q_+ = \frac{q_0 \alpha_-}{\alpha_- - \alpha_+} > 0$$

$$q_- = \frac{-q_0 \alpha_+}{\alpha_- - \alpha_+} < 0$$

since
 $\alpha_- - \alpha_+ < 0$
and
 α_- and
 α_+ are
both negative

32-52)

When overdamped, it can take a long time to reach zero because of "Molasses effect" - slow decline in spring to equilibrium.



b) Critically damped

$$\left(\frac{R}{2L}\right)^2 - \frac{1}{LC} = 0$$

$$\text{or } \left(\frac{R}{2L}\right)^2 = \frac{1}{LC} \quad \text{or } \frac{2L}{R} = \sqrt{LC}$$

In this case our two solutions collapse to one) $R_{\text{crit}} = 2\sqrt{\frac{L}{C}}$

$$q = q_0 e^{-t/\tau}$$

~~$$\tau = \frac{2L}{R}$$~~

$$\tau = 2L/R = \sqrt{LC}$$

Actually there must always be a 2nd solution — but our trial solution failed to find it in this special case.

real solution is a trick to guarantee it will always work.

The other solution is $te^{-t/2}$

Optional Reading

Math detail from Art - 403-404

$$\begin{aligned}
 q_2 &= q_1 \int \frac{e^{-\int \frac{P}{R} dt}}{q_1^2} dt \\
 &= e^{-t/2} \int \frac{e^{-\frac{R}{R} t}}{e^{-2t/2}} dt \\
 &= e^{-t/2} t
 \end{aligned}$$

Thus the full general solution is $q = e^{-t/2} (C_1 + C_2 t)$

32-54

We can confirm this is a solution

$$q' = e^{-t/RC} + \left(-\frac{1}{RC}\right)e^{-t/RC}$$

$$\begin{aligned} q'' &= \left(-\frac{1}{RC}\right)e^{-t/RC} + \left(\frac{1}{RC^2}\right)e^{-t/RC} \\ &\quad + \left(-\frac{1}{RC}\right)e^{-t/RC} \\ &= -\frac{2}{RC}e^{-t/RC} + \frac{e^{-t/RC}}{RC^2} \end{aligned}$$

$$Lq'' + q'R + \frac{q}{C} = 0$$

$$q'' + q' \frac{R}{L} + \frac{q}{LC} = 0$$

$$q'' + q' \frac{R}{L} + \frac{q}{LC} = 0$$

$$\left(-\frac{2}{RC}e^{-t/RC} + \frac{e^{-t/RC}}{RC^2}\right) + \left(\frac{2e^{-t/RC}}{C} - \frac{2}{RC^2}e^{-t/RC}t\right) + \frac{e^{-t/RC}}{C} = 0 \text{ confirmed}$$

So the full solution is

$$Q = q_0 e^{-t/\tau} + q_1 t e^{-t/\tau}$$

But we have to match the initial conditions.

$Q = q_0$ at $t = 0$ is already satisfied

$$I_0 = \left. \frac{dQ}{dt} \right|_0 = 0$$

$\frac{dQ}{dt}$
 $= \left(-\frac{q_0}{\tau} + \frac{q_1}{\tau} - \frac{q_1 t}{\tau^2}\right) e^{-t/\tau}$
 $= \frac{1}{\tau} \left(-q_0 + q_1 - \frac{q_1 t}{\tau}\right) e^{-t/\tau}$
 < 0
 and decays monotonically

$$\frac{dQ}{dt} = -\frac{1}{\tau} q_0 e^{-t/\tau} + \frac{q_1}{\tau} e^{-t/\tau} - \frac{1}{\tau} q_1 t e^{-t/\tau}$$

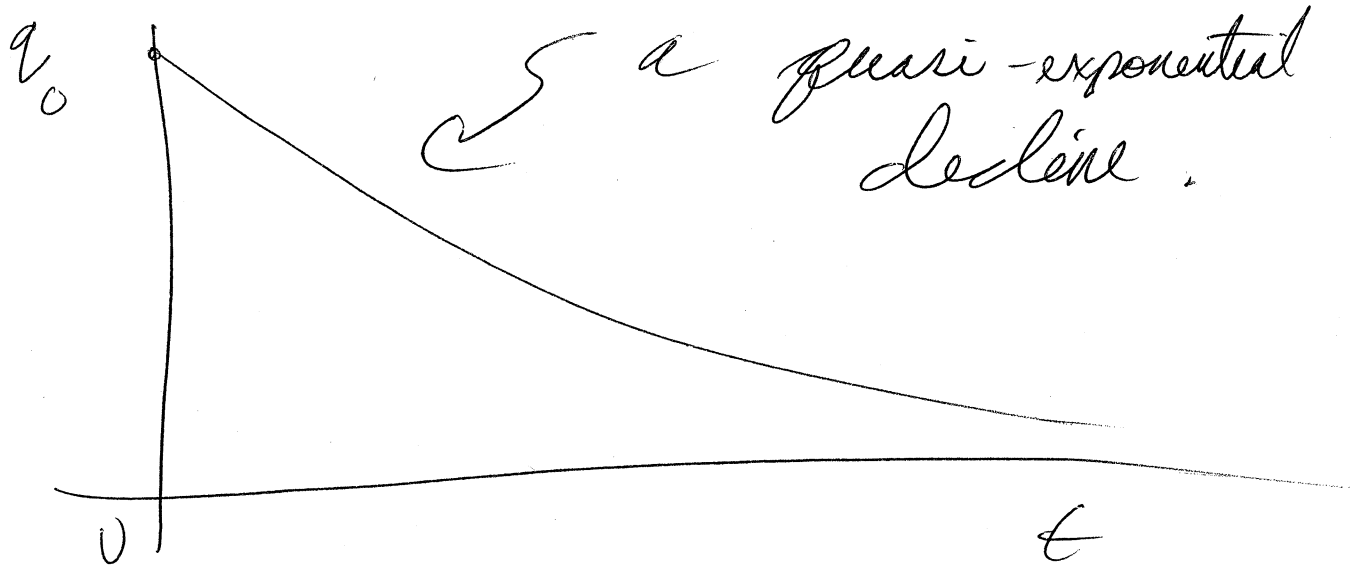
$$\left. \frac{dQ}{dt} \right|_{t=0} = -\frac{1}{\tau} q_0 + \frac{q_1}{\tau} = 0$$

$$q_1 = \frac{q_0}{\tau}$$

$$Q = q_0 \left(1 + \frac{t}{\tau}\right) e^{-t/\tau}$$

32-56

- Overdamped is slower decline by inductance effect.
- underdamped is slower decline by oscillations.



c) Underdamped case

$$\alpha_{\pm} = -\frac{R}{2L} \pm \sqrt{\left(\frac{R}{2L}\right)^2 - \frac{1}{LC}}$$

but now the discriminant is negative and α is a complex number.

$$\text{So } q = q_+ e^{\alpha_+ t} + q_- e^{\alpha_- t}$$

is an ~~not~~ ^{actual} solution to 32-57
the DE, but not
a "real" solution which
means not physical;

On the perspective of p. 32-69, the real part of the complex solution

But appropriate linear combinations of the two complex solutions gives two real solutions (really real solutions).

We omit details (for the moment)

$$q_v = (A \cos \omega t + B \sin \omega t) e^{-\frac{t}{\tau}}$$

$$\text{where } \tau = \frac{2L}{R}$$

$$\text{and } \omega = \sqrt{\frac{1}{LC} - \left(\frac{R}{2L}\right)^2} > 0$$

32-58

A and B are set
by our Initial
conditions.

$$A = q_0 \text{ clearly.}$$

$$\text{and } \frac{dq}{dt} = (q_0 \cos \omega t + B \sin \omega t) e^{-t/\tau} \left(-\frac{1}{\tau}\right) \\ + (-q_0 \omega \sin \omega t + B \omega \cos \omega t) e^{-t/\tau}$$

For $t = 0$

~~0 for t~~

$$0 = q_0 \left(-\frac{1}{\tau}\right) \text{ ~~0~~ } + B \omega$$

$$B = \frac{q_0}{\tau \omega} = \frac{q_0}{\sqrt{\frac{4L}{R^2 C} - 1}}$$

~~0~~

$$\left[\frac{L}{R^2 C} \right] = \frac{V/(A \cdot s)}{(V/A)^2 \cdot s} = \frac{A \cdot s}{C} = 1$$

unitless
as it should
be.

$$\text{If } \frac{4L}{R^2C} \gg 1,$$

32-59

$$\text{then } B \ll q_0$$

and this seems to be the case the text assumes.

or another way to look at it $\omega = 2\pi f$

$$= 2\pi / T \quad \left\{ \begin{array}{l} \text{period} \\ \text{of} \\ \text{oscillation} \end{array} \right.$$

$$\text{So if } T \ll 2\pi\tau \text{ or } \omega \text{ is big}$$

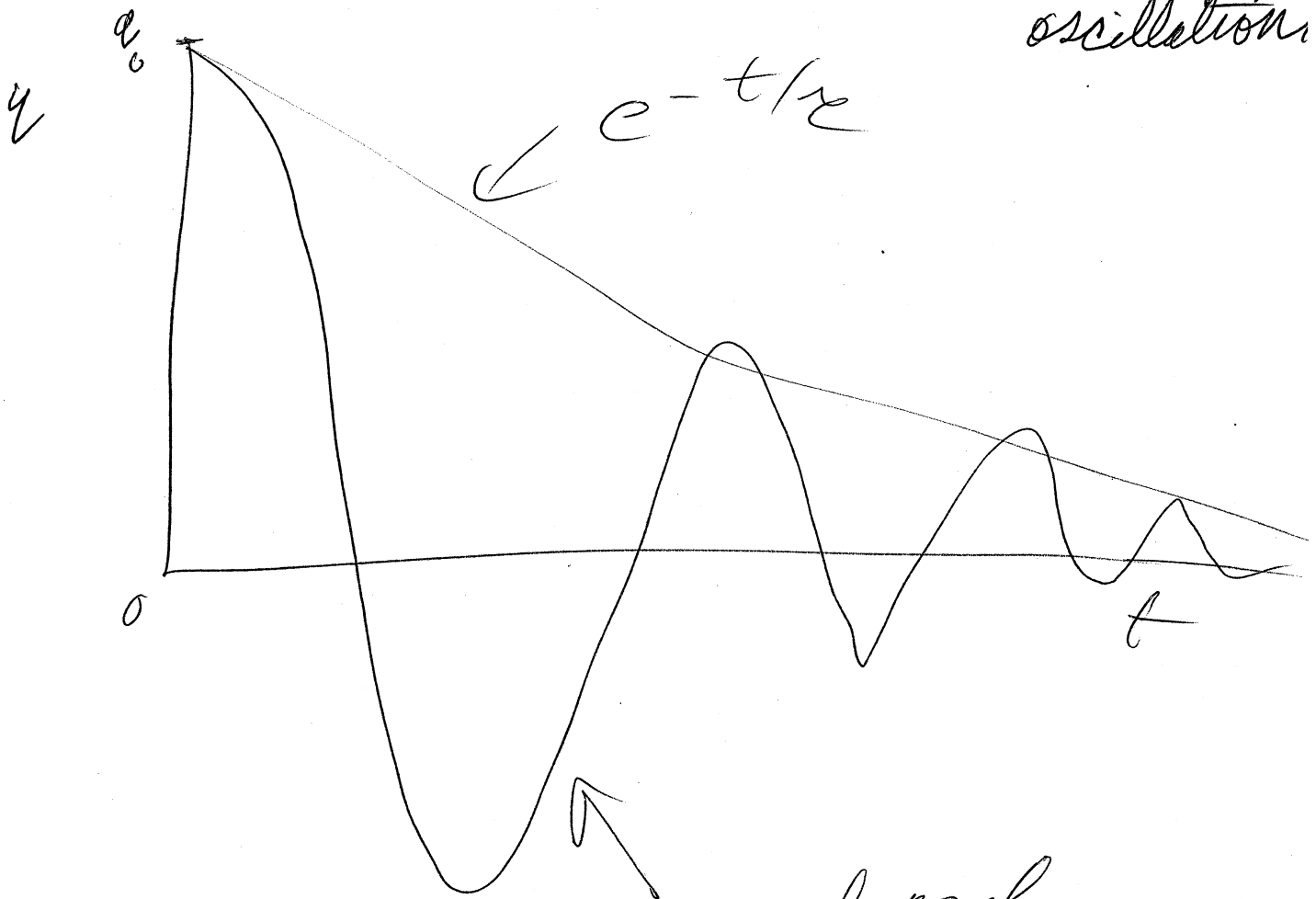
$$\text{then } B \ll q_0$$

$$\text{So } q = \left(q_0 \cos \omega t + \frac{q_0}{\epsilon \omega} \sin \omega t \right) e^{-t/\tau}$$

but for high frequency this term is ~~negligible~~ small.

32-60

In the underdamping case the decline is slow to zero because of oscillations.



enveloped
~~the~~ oscillations
- damped
oscillations.

R is essentially the damping parameter.

As R is reduced for fixed L & C 32-61

$$\alpha_{\pm} = -\frac{R}{2L} \pm \sqrt{\left(\frac{R}{2L}\right)^2 - \frac{1}{LC}}$$

the damping declines
from ~~over~~ underdamped
to critically damped
for $\left(\frac{R}{2L}\right)^2 - \frac{1}{LC} = 0$

$$\text{or } R = 2\sqrt{\frac{L}{C}} = R_{\text{crit}}$$

to underdamped

$$\text{for } R < 2\sqrt{\frac{L}{C}} = R_{\text{crit}}$$

32-62)

Mechanical analogies
- not exact ones

- Spring closed are usually
} overdamped.
} one doesn't want them
to close too quickly
and pop one on the nose.

- But for some reason
restaurant doors to the
kitchen that swing both
ways are a little overdamped
and oscillate a bit.

(I don't know why)

32-63

Optional further details

$$\alpha_{\pm} = -\frac{1}{\tau_{RL}} \pm \sqrt{\frac{1}{\tau_{RL}^2} - \frac{1}{\tau_{LC}^2}}$$

$$\tau_{RL} = \frac{RL}{R}$$

$$[\tau_{RL}] = \left[\frac{V/A(s)}{V/A} \right] = s \quad \checkmark$$

$$\tau_{LC} = \sqrt{LC}$$

~~$$[\tau_{LC}] = \left[\frac{V/A(s)}{V/A} \right]$$~~

$$[\tau_{LC}] = \sqrt{\frac{V}{A/s} \frac{C}{V}} = \sqrt{s^2} = s \quad \checkmark$$

$$\alpha_{\pm} = \left\{ -\frac{1}{\tau_{RL}} \left[1 \mp \sqrt{1 - \left(\frac{\tau_{RL}}{\tau_{LC}} \right)^2} \right] \right.$$

$$\left. -\frac{2}{\tau_{RL}} = -\frac{1}{\tau_{RL} 2} \right\}$$

lower case
for ~~the~~ case
and $\frac{\tau_{RL}}{\tau_{LC}} \ll 1$

$$\left. -\frac{1}{\tau_{RL}} \left(\frac{1}{2} \left(\frac{\tau_{RL}}{\tau_{LC}} \right)^2 \right) \right\}$$

$$= -\frac{1}{2} \frac{\tau_{RL}}{\tau_{LC}^2}$$

upper case
for ~~the~~ case
and $\frac{\tau_{RL}}{\tau_{LC}} \ll 1$

32-64)

and no decline time scale
(e-folding time)

are

$$\frac{\tau_{RL}}{2} \text{ and } \tau_{LC} \left[2 \left(\frac{\tau_{LC}}{\tau_{RL}} \right) \right]$$
$$= \frac{L}{R} = \tau_{RL*}$$

→]

and so this upper
case solution dominates
at late time.

$$= 2\sqrt{LC} \frac{\sqrt{LC}}{2LR}$$
$$= RC = \tau_{RC}$$
$$[\tau_{RC}] = \frac{1}{s} \cdot \frac{C}{V}$$
$$= s \checkmark$$

If $\tau_{RL} = \tau_{LC}$ or $R_{cut} = 2\sqrt{\frac{L}{C}}$
then

~~τ_{RL}~~ or ~~τ_{LC}~~ is the ~~same~~
e-folding time.

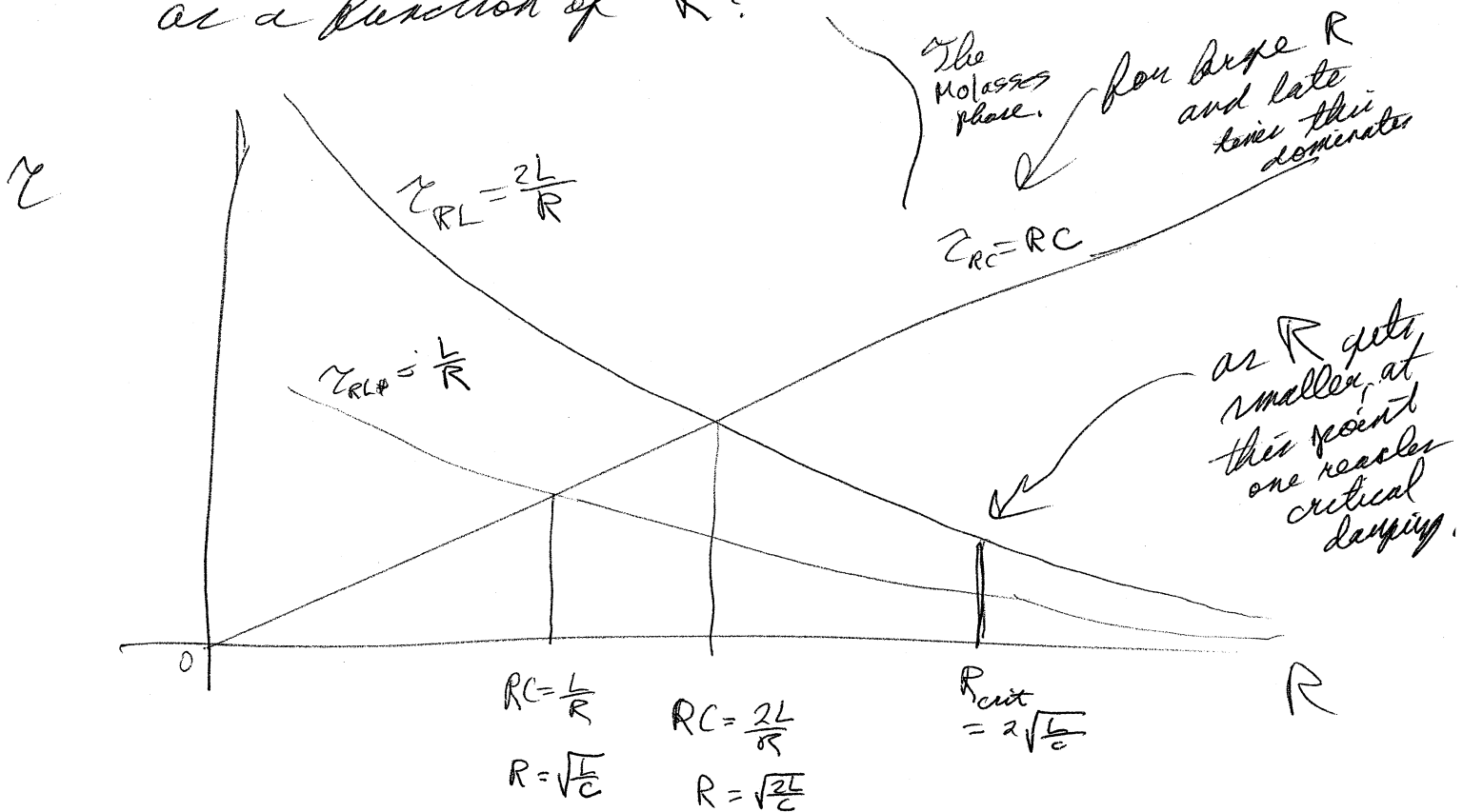
If $\zeta_{RL} < \zeta_{LC}$ 32-65

then $\zeta_{RL} = \frac{2L}{R}$ is

again the e-folding time,
but there is also the
oscillation with frequency

$$\omega = \sqrt{\frac{1}{LC} - \frac{1}{L^2 R^2}}$$

How do all ~~time scales~~ e-folding times behave
as a function of R ?



32-66

$$Z_{\text{general}} = \frac{1}{Z_{RL} + \sqrt{\frac{1}{Z_{RL}^2} - \frac{1}{Z_{LC}^2}}}$$

for $R \geq R_{\text{crit}}$

when $Z_{RL} = Z_{LC}$
 these are equal
 and $Z_{\text{gen}} = Z_{RL}$

$$= \frac{Z_{RL}}{1 + \sqrt{1 - \left(\frac{Z_{RL}}{Z_{LC}}\right)^2}}$$

$\frac{2L/R}{\sqrt{LC}}$

$$= \frac{2\sqrt{L/C}}{R} = \frac{R_{\text{crit}}}{R}$$

$$= \frac{2L}{R_{\text{crit}}} \frac{x}{1 + \sqrt{1 - x^2}}$$

↳

$$\frac{2L}{2\sqrt{LC}} \Rightarrow \sqrt{LC} = Z_{LC}$$

$$x \equiv \frac{R_{\text{crit}}}{R}$$

32-67

Where is the true stationary point?

$$f = \frac{x}{1 - \sqrt{1-x^2}}$$

$$\frac{df}{dx} = \frac{1}{1 - \sqrt{1-x^2}} - \frac{x \left(-\frac{1}{2}(1-x^2)^{-\frac{1}{2}}\right) 2x}{(1 - \sqrt{1-x^2})^2}$$

$$= \frac{1}{(1 - \sqrt{1-x^2})^2} \left[1 - \sqrt{1-x^2} - x^2 \sqrt{1-x^2} \right]$$

$$= \frac{1}{(\dots)} \frac{1}{\sqrt{1-x^2}} \left[\underbrace{\sqrt{1-x^2} - (1-x^2) + x^2}_{\sqrt{1-x^2} - 1} \right]$$

for a stationary point

$$\sqrt{1-x^2} - 1 = 0$$

$$1 - x^2 = 1$$

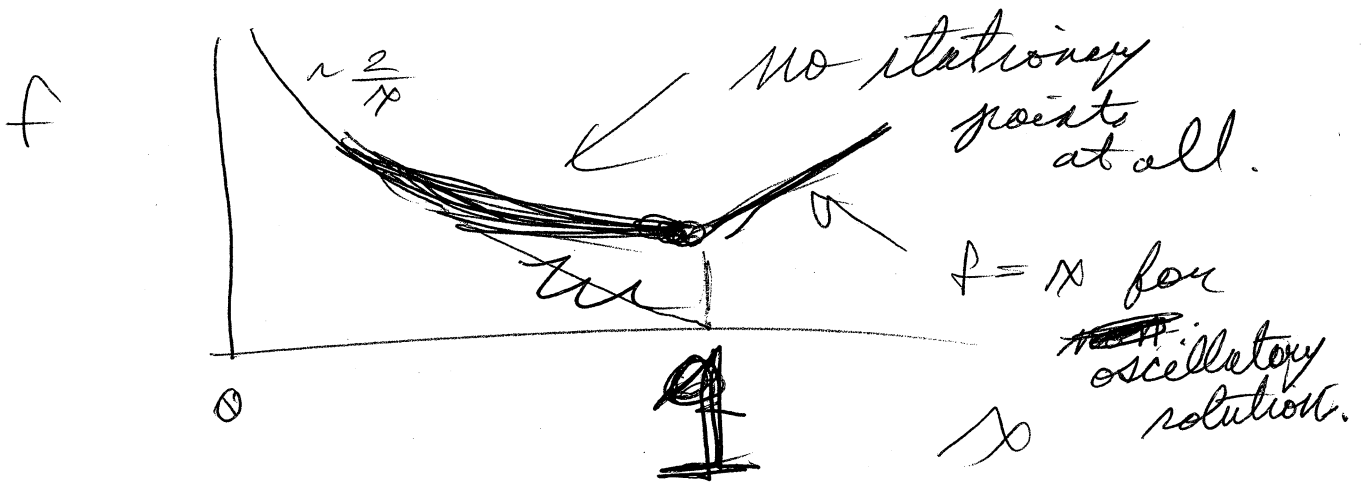
$$x^2 = 0, \text{ or } x = 0$$

but that's a bad point,

32-68

$$f(x) \approx \frac{x}{1 - (1 - \frac{1}{2}x^2)} \quad \text{for small } x.$$

$$= \frac{2}{x}$$



So as $x \rightarrow 0$, $R \rightarrow \infty$

the τ_{gen} increases without ~~out~~ bound from $x=1$
 on $x_{cut} \leq 1$

So there are no stationary points. So the actual minimum time scale is at $x_{cut} = 1$
 on $x \leq 1$

Now what about getting those real oscillatory solutions?

Well the complex solution we obtained by trial solution is

$$I = A e^{-t/\tau} e^{i\omega t} + B e^{-t/\tau} e^{-i\omega t}$$

where $\tau = \frac{2L}{R}$

and $\omega = \sqrt{\frac{1}{LC} - \left(\frac{R}{2L}\right)^2} > 0$

A and B are arbitrary so say we let $B \rightarrow +iB$ and take the real part of the solution which is also

32-70)

a solution of DE

— the real & imaginary parts of DE must separately solve the

DE \Rightarrow this is just part & parcel of complex number theory.

$$e^{i\omega t} = \cos \omega t + i \sin \omega t$$

by Euler's formula
Art - 264

$$y = (A \cos \omega t + B \sin \omega t) e^{-t/\tau}$$

Just as on p. 32-57.

S32.4 Mutual

32-71

Inductance

Somehow I omitted
this subject in its proper
place.

But there is not much
new.

— Self-inductance is
the ^{induced} emf in a circuit
or circuit device induced
by the ~~circuit itself~~ the current
in the circuit or device

Mutual-inductance is when
the induced emf in a circuit
or device is due to

32-72)

to a current elsewhere.

— usually one can consider it as the interaction between circuits.

→ This often just happens in a small way without any intention

— But in some cases transformers most obviously — it is a design feature

For Fixed in space circuit paths.

$$E_2 \propto \frac{d\bar{\Phi}_{12}}{dt} \propto \frac{dI_1}{dt}$$

$\bar{\Phi}_{12}$ is flux in 2 due to 1

— The proportionality constant is M (32-73)

$$E_2 = - M_{12} \frac{dI_1}{dt}$$

~~the~~ conventional minus
— the sense of E_2 can be deduced from Lenz's law.

The reverse situation occurs

$$E_1 = - M_{21} \frac{dI_2}{dt}$$

and it can be proven

(but I don't know how and it seems to be tricky)

32-74)

that $M_{12} = M_{21}$,

and no one can
just write M for
one ~~case~~ system.

No
proof
- we
have
faith

M depends on geometry
and on magnetic materials
that are used.

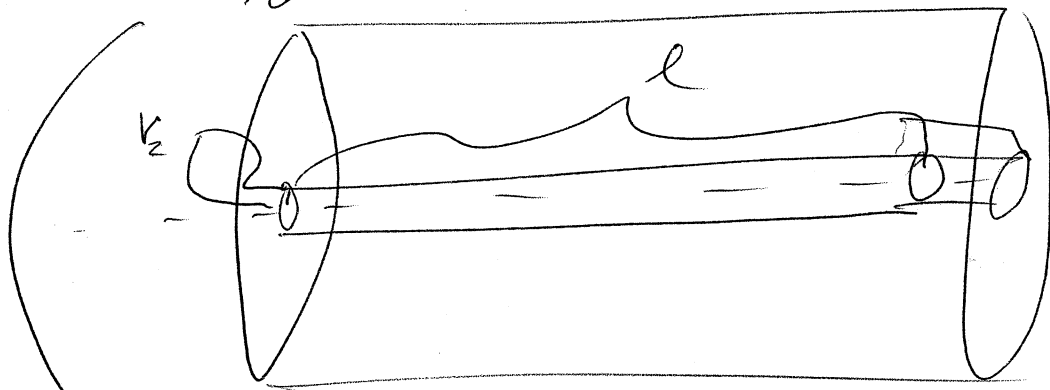
↳ in transformers
soft iron cores usually

↳ They do have a big
and important effect.

We'll just consider
one example case.

Two con-axial solenoids that we treat as ideal

32-79



this means $B = \mu_0 n I$

\uparrow \uparrow
 turns current
 per
 unit
 length

B is uniform inside and zero outside

→ due to any one of the solenoids

This is an infinite solenoid result, but we use it for finite ones in the ideal approximation.

$$\Phi_{12} = N_2 A_2 B_1 \leftarrow B_1 = \mu_0 n_1 I_1$$

Number of turns in solenoid 2 πr_2^2

32-76)

$$\Phi_{12} = \frac{N_2}{l} A_2 \mu_0 n_1 I_1$$

V_2 the volume of 2

$$= \mu_0 n_1 n_2 V_2 I_1$$

$$\mathcal{E}_2 = -\frac{d\Phi_{12}}{dt} = -\mu_0 n_1 n_2 V_2 \frac{dI_1}{dt}$$

$$\therefore M_{12} = \mu_0 n_1 n_2 V_2 \quad (\text{TM-977})$$

What of M_{21} ?

$$\Phi_{21} = N_1 A_2 B_2$$

$$\mu_0 n_2 I_2$$

B_2 only extends
over A_2 and
is zero outside

$$= n_1 l A_2 \mu_0 n_2 I_2$$

$$= \mu_0 n_1 n_2 V_2 I_2$$

$$\varepsilon_1 = - \underbrace{\mu_0 n_1 n_2 V_2}_{\text{}} \frac{dI_2}{dt}$$

32-77

$$\begin{aligned} M_{21} &= \mu_0 n_1 n_2 V_2 \\ &= M_{12} \end{aligned}$$

So we've confirmed the general result in this special case.

32-78

— Mutual inductance is tricky since one can have feedback

1 induces a current in 2

which induces an emf in 1

which affects the current in 1

which changes the induced current in 2, and so on

Which could be regarded as part of self-inductance?
I'm not sure.

— Nature presumably sorts this out quickly.

— But I'm not sure we know how to calculate all this easily in