## Intro Physics Semester I

Name:
Homework III: Thermodynamics III: Entropy and 2nd Law One or two full answer questions will be marked. There will also be a mark for completeness. Homeworks are due usually the day after the chapter they are for is finished. Solutions will be posted soon thereafter. The solutions are intended to be (but not necessarily are) super-perfect and often go beyond a fully correct answer.

## Answer Table

|  | a | b | c | d | e |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1. | O | O | O | O | O |
| 2. | O | O | O | O | O |
| 3. | O | O | O | O | O |
| 4. | O | O | O | O | O |
| 5. | O | O | O | O | O |
| 6. | O | O | O | O | O |
| 7. | O | O | O | O | O |
| 8. | O | O | O | O | O |
| 9. | O | O | O | O | O |
| 10. | O | O | O | O | O |
| 11. | O | O | O | O | O |
| 12. | O | O | O | O | O |
| 13. | O | O | O | O | O |
| 14. | O | O | O | O | O |
| 15. | O | O | O | O | O |
| 16. | O | O | O | O | O |
| 17. | O | O | O | O | O |
| 18. | O | O | O | O | O |
| 19. | O | O | O | O | O |
| 20. | O | O | O | O | O |
| 21. | O | O | O | O | O |
| 22. | O | O | O | O | O |
| 23. | O | O | O | O | O |
| 24. | O | O | O | O | O |
| 25. | O | O | O | O | O |
| 26. | O | O | O | O | O |
| 27. | O | O | O | O | O |
| 28. | O | O | O | O | O |
| 29. | O | O | O | O | O |
| 30. | O | O | O | O | O |

Name:

|  | a | b | c | d | e |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 31. | O | O | O | O | O |
| 32. | O | O | O | O | O |
| 33. | O | O | O | O | O |
| 34. | O | O | O | O | O |
| 35. | O | O | O | O | O |
| 36. | O | O | O | O | O |
| 37. | O | O | O | O | O |
| 38. | O | O | O | O | O |
| 39. | O | O | O | O | O |
| 40. | O | O | O | O | O |
| 41. | O | O | O | O | O |
| 42. | O | O | O | O | O |
| 43. | O | O | O | O | O |
| 44. | O | O | O | O | O |
| 45. | O | O | O | O | O |
| 46. | O | O | O | O | O |
| 47. | O | O | O | O | O |
| 48. | O | O | O | O | O |
| 49. | O | O | O | O | O |
| 50. | O | O | O | O | O |
| 51. | O | O | O | O | O |
| 52. | O | O | O | O | O |
| 53. | O | O | O | O | O |
| 54. | O | O | O | O | O |
| 55. | O | O | O | O | O |
| 56. | O | O | O | O | O |
| 57. | O | O | O | O | O |
| 58. | O | O | O | O | O |
| 59. | O | O | O | O | O |
| 60. | O | O | O | O | O |

1. "Let's play Jeopardy! For $\$ 100$, the answer is: A device that operates in a cycle. It extracts heat from a hot reservoir and converts some fraction of this heat into macroscopic work and rejects the rest of the heat to a cold reservoir. The hot reservoir is at higher temperature than the cold resevoir as the names suggest."
What is a $\qquad$ , Alex?
a) working fluid
b) piston
c) cylinder
d) refrigerator
e) heat engine
2. The three main components of a heat engine are a hot reservoir, a cold reservoir, and a $\qquad$ .
The $\qquad$ is a substance sample (usually a gas at least part of the time during an engine cycle) that absorbs heat from a hot reservior, rejects heat to a cold and performs the macroscopic work of the engine. At the end of an engine cycle, the $\qquad$ has returned to its original thermodynamic state.
a) valve
b) idling stuff
c) working fluid
d) engine fluid
e) radiator
3. An example of a heat engine is a/an:
a) fire.
b) internal combustion engine.
c) electric motor.
d) common household refrigerator.
e) bicycle.
4. "Let's play Jeopardy! For $\$ 100$, the answer is: A device that operates in a cycle. It extracts heat from a cold reservoir and rejects the rest of the heat hot reservoir. This process requires an input of work. The work energy is rejected to the hot reservoir too. The device needs a working fluid that absorbs and rejects the heat and has work done on it. At the end of a cycle, the working fluid has returned to its orginal state. The device is a heat engine run in reverse. However, there are very few heat engines that are designed to run in reverse."

What is a $\qquad$ , Alex?
a) working fluid
b) piston
c) cylinder
d) refrigerator
e) heat engine
5. The heat a refrigerator absorbs from its cold bath (or cold reservoir) is:
a) more than the heat is reject to its hot bath.
b) less than the heat it rejects to its hot bath.
c) zero.
d) infinite.
e) the same as it rejects to its hot bath.
6. The performance of heat engines and refrigerators need to be evaluated in many ways since they are used in many ways. However, a generally useful performance measure for a heat engine is the efficiency defined by

$$
\varepsilon=\frac{W}{Q_{\mathrm{H}}}=\frac{Q_{\mathrm{H}}-Q_{\mathrm{C}}}{Q_{\mathrm{H}}}=1-\frac{Q_{\mathrm{C}}}{Q_{\mathrm{H}}}
$$

where $W$ is the work output, $Q_{\mathrm{H}}$ is the heat absorbed from the hot bath, and $Q_{\mathrm{C}}$ is the heat rejected to the cold bath. Two generally useful performance measures for a refrigerator are the heating and cooling coefficients of performance:

$$
\eta_{\text {heating }}=\frac{Q_{\mathrm{H}}}{W}=\frac{Q_{\mathrm{H}}}{Q_{\mathrm{H}}-Q_{\mathrm{C}}}=\frac{1}{1-Q_{\mathrm{C}} / Q_{\mathrm{H}}}=\frac{1}{\varepsilon}
$$

and

$$
\eta_{\text {cooling }}=\frac{Q_{\mathrm{C}}}{W}=\frac{Q_{\mathrm{H}}-W}{W}=\frac{1}{\varepsilon}-1=\eta_{\text {heating }}-1
$$

where $W$ is the work input, $Q_{\mathrm{H}}$ is the heat rejected to the hot bath, $Q_{\mathrm{C}}$ is the heat absorbed from the cold bath, and $\varepsilon$ is just a parameter in these equations not an efficiency since they are refrigerators, not heat engines. Given $Q_{\mathrm{C}} / Q_{\mathrm{H}}=1 / 2$, what are the values of $\varepsilon, \eta_{\text {heating }}$, and $\eta_{\text {cooling }}$
a) $1 / 2,2,1 / 2$.
b) $2,1 / 2,2$.
c) $1 / 2,2,1$.
d) $2,2,1$.
e) $1,1,0$.
7. The argument that a reversible heat engine - if it exists-is the most efficient heat engine and highest performance refrigerator (when run in reverse) is as follows. Imagine two identical reversibles: one runs forward as a heat engine and one runs in reverse as a fridge. For the forward/reverse engine let $W$ be the work output/input, $Q_{\mathrm{H}}$ be the heat absorbed from/rejected to the hot bath, and $Q_{\mathrm{C}}$ be the heat rejected to/absorbed from the cold bath. We use the work output of the forward engine to drive the
reverse engine. From an outside perspective, nothing happens averaged over an engine cycle. No net work is done and no net heat leaves or enters the baths.

Now imagine a more efficient heat engine than the reversible and use it to replace the forward reversible. Scale it to reject $Q_{\mathrm{C}}$. Since it is more efficient, it absorbs $Q_{\mathrm{H}}^{\prime}>Q_{\mathrm{H}}$ and does work $W^{\prime}>W$. Now the net effect over a cycle is that net work $W^{\prime}-W>0$ is done and net heat $Q_{\mathrm{H}}^{\prime}-Q_{\mathrm{H}}$ is removed from the hot bath and there is no net change to the cold bath. Thus, an amount of heat $Q_{\mathrm{H}}^{\prime}-Q_{\mathrm{H}}$ is turned entirely into work with no other effect. This process is just never observed in nature and no one has ever been able to construct anything like it. It is a reasonable, but not incontrovertible, conclusion that the more efficient heat engine is impossible and the reversible - if it exists-must be the highest efficiency engine.

Now imagine a higher performance refrigerator than the reversible and use it to replace the reverse reversible. Scale it to use work $W$. Since it is higher performance, it absorbs $Q_{\mathrm{C}}^{\prime}>Q_{\mathrm{C}}$ from the cold bath and rejects heat $Q_{\mathrm{H}}^{\prime}>Q_{\mathrm{H}}$ to the hot bath. Now the net effect over a cycle is that net work is zero and net heat $Q_{\mathrm{H}}^{\prime}-Q_{\mathrm{H}}=Q_{\mathrm{C}}^{\prime}>Q_{\mathrm{C}}$ is removed from the cold bath and transferred to the hot bath. This process is just never observed in nature and no one has ever been able to construct anything like it. Heat does not spontaneously flow from hot to cold. It is a reasonable, but not incontrovertible, conclusion that the higher performance refrigerator is impossible and the reversible - if it exists-must be the highest performance refrigerator.

As a matter of fact, the $\qquad$ of thermodynamics (which is an axiom of thermodynamics) dictates the non-existence of the more efficient engine and the higher performance refrigerator, and therefore leads to the conclusion the reversible - if it exists - must be the most efficient heat engine and highest performance refrigerator.
a) zeroth law
b) 1st law
c) 2nd law
d) 3rd law
e) 4th law

## Equation Sheet for Introductory Physics Calculus-Based

This equation sheet is intended for students writing tests or reviewing material. Therefore it is neither intended to be complete nor completely explicit. There are fewer symbols than variables, and so some symbols must be used for different things: context must distinguish.

The equations are mnemonic. Students are expected to understand how to interpret and use them.

## 1 Constants

$$
\begin{aligned}
c & =2.99792458 \times 10^{8} \mathrm{~m} / \mathrm{s} \approx 2.998 \times 10^{8} \mathrm{~m} / \mathrm{s} \approx 3 \times 10^{8} \mathrm{~m} / \mathrm{s} \approx 1 \mathrm{lyr} / \mathrm{yr} \approx 1 \mathrm{ft} / \mathrm{ns} \quad \text { exact by definition } \\
e & =1.602176487(40) \times 10^{-19} \mathrm{C} \\
G & =6.67384(80) \times 10^{-11} \mathrm{~N} \mathrm{~m}^{2} / \mathrm{kg}^{2} \quad(2012, \mathrm{CODATA}) \\
g & =9.8 \mathrm{~m} / \mathrm{s}^{2} \quad \text { fiducial value } \\
k & =\frac{1}{4 \pi \varepsilon_{0}}=8.987551787 \ldots \times 10^{9} \approx 8.99 \times 10^{9} \approx 10^{10} \mathrm{~N} \mathrm{~m}^{2} / \mathrm{C}^{2} \text { exact by definition } \\
k_{\text {Boltzmann }} & =1.3806504(24) \times 10^{-23} \mathrm{~J} / \mathrm{K}=0.8617343(15) \times 10^{-4} \mathrm{eV} / \mathrm{K} \approx 10^{-4} \mathrm{eV} / \mathrm{K} \\
m_{e} & =9.10938215(45) \times 10^{-31} \mathrm{~kg}=0.510998910(13) \mathrm{MeV} \\
m_{p} & =1.672621637(83) \times 10^{-27} \mathrm{~kg}=938.272013(23), \mathrm{MeV} \\
\varepsilon_{0} & =\frac{1}{\mu_{0} c^{2}}=8.8541878176 \ldots \times 10^{-12} \mathrm{C}^{2} /\left(\mathrm{N} \mathrm{~m}^{2}\right) \approx 10^{-11} \quad \text { vacuum permittivity (exact by definition) } \\
\mu_{0} & =4 \pi \times 10^{-7} \mathrm{~N} / \mathrm{A}^{2} \quad \text { exact by definition }
\end{aligned}
$$

## 2 Geometrical Formulae

$$
\begin{gathered}
C_{\text {cir }}=2 \pi r \quad A_{\text {cir }}=\pi r^{2} \quad A_{\mathrm{sph}}=4 \pi r^{2} \quad V_{\mathrm{sph}}=\frac{4}{3} \pi r^{3} \\
\Omega_{\text {sphere }}=4 \pi \quad d \Omega=\sin \theta d \theta d \phi
\end{gathered}
$$

3 Trigonometry Formulae

$$
\begin{gathered}
\frac{x}{r}=\cos \theta \quad \frac{y}{r}=\sin \theta \quad \frac{y}{x}=\tan \theta=\frac{\sin \theta}{\cos \theta} \quad \cos ^{2} \theta+\sin ^{2} \theta=1 \\
\csc \theta=\frac{1}{\sin \theta} \quad \sec \theta=\frac{1}{\cos \theta} \quad \cot \theta=\frac{1}{\tan \theta} \\
c^{2}=a^{2}+b^{2} \quad c=\sqrt{a^{2}+b^{2}-2 a b \cos \theta_{c}} \quad \frac{\sin \theta_{a}}{a}=\frac{\sin \theta_{b}}{b}=\frac{\sin \theta_{c}}{c} \\
f(\theta)=f\left(\theta+360^{\circ}\right) \\
\sin \left(\theta+180^{\circ}\right)=-\sin (\theta) \quad \cos \left(\theta+180^{\circ}\right)=-\cos (\theta) \quad \tan \left(\theta+180^{\circ}\right)=\tan (\theta) \\
\sin (-\theta)=-\sin (\theta) \quad \cos (-\theta)=\cos (\theta) \quad \tan (-\theta)=-\tan (\theta)
\end{gathered}
$$

$$
\begin{aligned}
& \sin \left(\theta+90^{\circ}\right)=\cos (\theta) \quad \cos \left(\theta+90^{\circ}\right)=-\sin (\theta) \quad \tan \left(\theta+90^{\circ}\right)=-\tan (\theta) \\
& \sin \left(180^{\circ}-\theta\right)=\sin (\theta) \quad \cos \left(180^{\circ}-\theta\right)=-\cos (\theta) \quad \tan \left(180^{\circ}-\theta\right)=-\tan (\theta) \\
& \sin \left(90^{\circ}-\theta\right)=\cos (\theta) \quad \cos \left(90^{\circ}-\theta\right)=\sin (\theta) \quad \tan \left(90^{\circ}-\theta\right)=\frac{1}{\tan (\theta)}=\cot (\theta) \\
& \sin (a+b)=\sin (a) \cos (b)+\cos (a) \sin (b) \quad \cos (a+b)=\cos (a) \cos (b)-\sin (a) \sin (b) \\
& \sin (2 a)=2 \sin (a) \cos (a) \quad \cos (2 a)=\cos ^{2}(a)-\sin ^{2}(a) \\
& \sin (a) \sin (b)=\frac{1}{2}[\cos (a-b)-\cos (a+b)] \quad \cos (a) \cos (b)=\frac{1}{2}[\cos (a-b)+\cos (a+b)] \\
& \sin (a) \cos (b)=\frac{1}{2}[\sin (a-b)+\sin (a+b)] \\
& \sin ^{2} \theta=\frac{1}{2}[1-\cos (2 \theta)] \quad \cos ^{2} \theta=\frac{1}{2}[1+\cos (2 \theta)] \quad \sin (a) \cos (a)=\frac{1}{2} \sin (2 a) \\
& \cos (x)-\cos (y)=-2 \sin \left(\frac{x+y}{2}\right) \sin \left(\frac{x-y}{2}\right) \\
& \cos (x)+\cos (y)=2 \cos \left(\frac{x+y}{2}\right) \cos \left(\frac{x-y}{2}\right) \\
& \sin (x)+\sin (y)=2 \sin \left(\frac{x+y}{2}\right) \cos \left(\frac{x-y}{2}\right)
\end{aligned}
$$

## 4 Approximation Formulae

$$
\begin{aligned}
\frac{\Delta f}{\Delta x} \approx \frac{d f}{d x} \quad \frac{1}{1-x} \approx 1+x:(x \ll 1) \\
\sin \theta \approx \theta \quad \tan \theta \approx \theta \quad \cos \theta \approx 1-\frac{1}{2} \theta^{2} \quad \text { all for } \theta \ll 1
\end{aligned}
$$

## 5 Quadratic Formula

If

$$
0=a x^{2}+b x+c, \quad \text { then } \quad x=\frac{-b \pm \sqrt{b^{2}-4 a c}}{2 a}=-\frac{b}{2 a} \pm \sqrt{\left(\frac{b}{2 a}\right)^{2}-\frac{c}{a}}
$$

## 6 Vector Formulae

$$
\begin{gathered}
a=|\vec{a}|=\sqrt{a_{x}^{2}+a_{y}^{2}} \quad \theta=\tan ^{-1}\left(\frac{a_{y}}{a_{x}}\right)+\pi ? \quad \vec{a}+\vec{b}=\left(a_{x}+b_{x}, a_{y}+b_{y}\right) \\
a=|\vec{a}|=\sqrt{a_{x}^{2}+a_{y}^{2}+a_{z}^{2}} \quad \phi=\tan ^{-1}\left(\frac{a_{y}}{a_{x}}\right)+\pi ? \quad \theta=\cos ^{-1}\left(\frac{a_{z}}{a}\right) \\
\vec{a}+\vec{b}=\left(a_{x}+b_{x}, a_{y}+b_{y}, a_{z}+b_{z}\right) \\
\vec{a} \cdot \vec{b}=a b \cos \theta=a_{x} b_{x}+a_{y} b_{y}+a_{z} b_{z} \\
\vec{c}=\vec{a} \times \vec{b}=a b \sin (\theta) \hat{c}=\left(a_{y} b_{z}-b_{y} a_{z}, a_{z} b_{x}-b_{z} a_{x}, a_{x} b_{y}-b_{x} a_{y}\right)
\end{gathered}
$$

7 Differentiation and Integration Formulae

$$
\frac{d\left(x^{p}\right)}{d x}=p x^{p-1} \quad \text { except for } p=0 ; \quad \frac{d\left(x^{0}\right)}{d x}=0 \quad \frac{d(\ln |x|)}{d x}=\frac{1}{x}
$$

Taylor's series $\quad f(x)=\sum_{n=0}^{\infty} \frac{\left(x-x_{0}\right)^{n}}{n!} f^{(n)}\left(x_{0}\right)$

$$
=f\left(x_{0}\right)+\left(x-x_{0}\right) f^{(1)}\left(x_{0}\right)+\frac{\left(x-x_{0}\right)^{2}}{2!} f^{(2)}\left(x_{0}\right)+\frac{\left(x-x_{0}\right)^{3}}{3!} f^{(3)}\left(x_{0}\right)+\ldots
$$

$$
\int_{a}^{b} f(x) d x=\left.F(x)\right|_{a} ^{b}=F(b)-F(a) \quad \text { where } \quad \frac{d F(x)}{d x}=f(x)
$$

$$
\int x^{n} d x=\frac{x^{n+1}}{n+1} \quad \text { except for } n=-1 ; \quad \int \frac{1}{x} d x=\ln |x|
$$

## 8 One-Dimensional Kinematics

$$
\begin{gathered}
v_{\mathrm{avg}}=\frac{\Delta x}{\Delta t} \quad v=\frac{d x}{d t} \quad a_{\mathrm{avg}}=\frac{\Delta v}{\Delta t} \quad a=\frac{d v}{d t}=\frac{d^{2} x}{d t^{2}} \\
v=a t+v_{0} \quad x=\frac{1}{2} a t^{2}+v_{0} t+x_{0} \quad v^{2}=v_{0}^{2}+2 a\left(x-x_{0}\right) \\
x=\frac{1}{2}\left(v_{0}+v\right) t+x_{0} \quad x=-\frac{1}{2} a t^{2}+v t+x_{0} \quad g=9.8 \mathrm{~m} / \mathrm{s}^{2}
\end{gathered}
$$

$$
\begin{array}{r}
x_{\text {rel }}=x_{2}-x_{1} \quad v_{\text {rel }}=v_{2}-v_{1} \quad a_{\text {rel }}=a_{2}-a_{1} \\
x^{\prime}=x-v_{\text {frame }} t \quad v^{\prime}=v-v_{\text {frame }} \quad a^{\prime}=a
\end{array}
$$

9 Two- and Three-Dimensional Kinematics: General

$$
\vec{v}_{\text {avg }}=\frac{\Delta \vec{r}}{\Delta t} \quad \vec{v}=\frac{d \vec{r}}{d t} \quad \vec{a}_{\mathrm{avg}}=\frac{\Delta \vec{v}}{\Delta t} \quad \vec{a}=\frac{d \vec{v}}{d t}=\frac{d^{2} \vec{r}}{d t^{2}}
$$

## 10 Projectile Motion

$$
\begin{gathered}
x=v_{x, 0} t \quad y=-\frac{1}{2} g t^{2}+v_{y, 0} t+y_{0} \quad v_{x, 0}=v_{0} \cos \theta \quad v_{y, 0}=v_{0} \sin \theta \\
t=\frac{x}{v_{x, 0}}=\frac{x}{v_{0} \cos \theta} \quad y=y_{0}+x \tan \theta-\frac{x^{2} g}{2 v_{0}^{2} \cos ^{2} \theta} \\
x_{\text {for } y \max }=\frac{v_{0}^{2} \sin \theta \cos \theta}{g} \quad y_{\text {max }}=y_{0}+\frac{v_{0}^{2} \sin ^{2} \theta}{2 g} \\
x\left(y=y_{0}\right)=\frac{2 v_{0}^{2} \sin \theta \cos \theta}{g}=\frac{v_{0}^{2} \sin (2 \theta)}{g} \quad \theta_{\text {for } \max }=\frac{\pi}{4} \quad x_{\max }\left(y=y_{0}\right)=\frac{v_{0}^{2}}{g} \\
x(\theta=0)= \pm v_{0} \sqrt{\frac{2\left(y_{0}-y\right)}{g}} \quad t(\theta=0)=\sqrt{\frac{2\left(y_{0}-y\right)}{g}}
\end{gathered}
$$

11 Relative Motion

$$
\vec{r}=\vec{r}_{2}-\vec{r}_{1} \quad \vec{v}=\vec{v}_{2}-\vec{v}_{1} \quad \vec{a}=\vec{a}_{2}-\vec{a}_{1}
$$

12 Polar Coordinate Motion and Uniform Circular Motion

$$
\begin{gathered}
\omega=\frac{d \theta}{d t} \quad \alpha=\frac{d \omega}{d t}=\frac{d^{2} \theta}{d t^{2}} \\
\vec{r}=r \hat{r} \quad \vec{v}=\frac{d \vec{r}}{d t}=\frac{d r}{d t} \hat{r}+r \omega \hat{\theta} \quad \vec{a}=\frac{d^{2} \vec{r}}{d t^{2}}=\left(\frac{d^{2} r}{d t^{2}}-r \omega^{2}\right) \hat{r}+\left(r \alpha+2 \frac{d r}{d t} \omega\right) \hat{\theta} \\
\vec{v}=r \omega \hat{\theta} \quad v=r \omega \quad a_{\tan }=r \alpha \\
\vec{a}_{\text {centripetal }}=-\frac{v^{2}}{r} \hat{r}=-r \omega^{2} \hat{r} \quad a_{\text {centripetal }}=\frac{v^{2}}{r}=r \omega^{2}=v \omega
\end{gathered}
$$

## 13 Very Basic Newtonian Physics

$$
\begin{aligned}
& \vec{r}_{\mathrm{cm}}=\frac{\sum_{i} m_{i} \vec{r}_{i}}{m_{\text {total }}}=\frac{\sum_{\mathrm{sub}} m_{\mathrm{sub}} \vec{r}_{\mathrm{cm} \mathrm{sub}}}{m_{\text {total }}} \quad \vec{v}_{\mathrm{cm}}=\frac{\sum_{i} m_{i} \vec{v}_{i}}{m_{\text {total }}} \quad \vec{a}_{\mathrm{cm}}=\frac{\sum_{i} m_{i} \vec{a}_{i}}{m_{\text {total }}} \\
& \vec{r}_{\mathrm{cm}}=\frac{\int_{V} \rho(\vec{r}) \vec{r} d V}{m_{\text {total }}} \\
& \vec{F}_{\text {net }}=m \vec{a} \quad \vec{F}_{21}=-\vec{F}_{12} \quad F_{g}=m g \quad g=9.8 \mathrm{~m} / \mathrm{s}^{2} \\
& \vec{F}_{\text {normal }}=-\vec{F}_{\text {applied }} \quad F_{\text {linear }}=-k x \\
& f_{\text {normal }}=\frac{T}{r} \quad T=T_{0}-F_{\text {parallel }}(s) \quad T=T_{0} \\
& F_{\mathrm{f} \text { static }}=\min \left(F_{\text {applied }}, F_{\mathrm{f} \text { static max }}\right) \quad F_{\mathrm{f} \text { static max }}=\mu_{\text {static }} F_{\mathrm{N}} \quad F_{\mathrm{f} \text { kinetic }}=\mu_{\text {kinetic }} F_{\mathrm{N}} \\
& v_{\text {tangential }}=r \omega=r \frac{d \theta}{d t} \quad a_{\text {tangential }}=r \alpha=r \frac{d \omega}{d t}=r \frac{d^{2} \theta}{d t^{2}} \\
& \vec{a}_{\text {centripetal }}=-\frac{v^{2}}{r} \hat{r} \quad \vec{F}_{\text {centripetal }}=-m \frac{v^{2}}{r} \hat{r} \\
& F_{\mathrm{drag}, \text { lin }}=b v \quad v_{\mathrm{T}}=\frac{m g}{b} \quad \tau=\frac{v_{\mathrm{T}}}{g}=\frac{m}{b} \quad v=v_{\mathrm{T}}\left(1-e^{-t / \tau}\right) \\
& F_{\text {drag,quad }}=b v^{2}=\frac{1}{2} C \rho A v^{2} \quad v_{\mathrm{T}}=\sqrt{\frac{m g}{b}}
\end{aligned}
$$

## 14 Energy and Work

$$
\begin{gathered}
d W=\vec{F} \cdot d \vec{s} \quad W=\int \vec{F} \cdot d \vec{s} \quad K E=\frac{1}{2} m v^{2} \quad E_{\text {mechanical }}=K E+P E \\
P_{\mathrm{avg}}=\frac{\Delta W}{\Delta t} \quad P=\frac{d W}{d t} \quad P=\vec{F} \cdot \vec{v}
\end{gathered}
$$

$\Delta K E=W_{\text {net }} \quad \Delta P E_{\text {of a conservative force }}=-W_{\text {by a conservative force }} \quad \Delta E=W_{\text {nonconservative }}$

$$
F=-\frac{d P E}{d x} \quad \vec{F}=-\nabla P E \quad P E=\frac{1}{2} k x^{2} \quad P E=m g y
$$

$$
\begin{gathered}
\vec{F}_{\mathrm{net}}=m \vec{a}_{\mathrm{cm}} \quad \Delta K E_{\mathrm{cm}}=W_{\mathrm{net}, \text { external }} \quad \Delta E_{\mathrm{cm}}=W_{\mathrm{not}} \\
\vec{p}=m \vec{v} \quad \vec{F}_{\mathrm{net}}=\frac{d \vec{p}}{d t} \quad \vec{F}_{\mathrm{net}}=\frac{d \vec{p}_{\mathrm{total}}}{d t} \\
m \vec{a}_{\mathrm{cm}}=\vec{F}_{\text {net non-flux }}+\left(\vec{v}_{\mathrm{flux}}-\vec{v}_{\mathrm{cm}}\right) \frac{d m}{d t}=\vec{F}_{\text {net non-flux }}+\vec{v}_{\mathrm{rel}} \frac{d m}{d t} \\
v=v_{0}+v_{\mathrm{ex}} \ln \left(\frac{m_{0}}{m}\right) \quad \text { rocket in free space }
\end{gathered}
$$

## 16 Collisions

$$
\begin{gathered}
\vec{I}=\int_{\Delta t} \vec{F}(t) d t \quad \vec{F}_{\mathrm{avg}}=\frac{\vec{I}}{\Delta t} \quad \Delta p=\vec{I}_{\text {net }} \\
\vec{p}_{1 i}+\vec{p}_{2 i}=\vec{p}_{1 f}+\vec{p}_{2 f} \quad \vec{v}_{\mathrm{cm}}=\frac{\vec{p}_{1}+\vec{p}_{2}}{m_{\text {total }}} \\
K E_{\text {total } f}=K E_{\text {total } i} \quad \text { 1-d Elastic Collision Expression } \\
v_{1^{\prime}}=\frac{\left(m_{1}-m_{2}\right) v_{1}+2 m_{2} v_{2}}{m_{1}+m_{2}} \quad \text { 1-d Elastic Collision Expression } \\
v_{2^{\prime}}-v_{1^{\prime}}=-\left(v_{2}-v_{1}\right) \quad v_{\text {rel }}=-v_{\text {rel }} \quad \text { 1-d Elastic Collision Expressions }
\end{gathered}
$$

17 Rotational Kinematics

$$
\begin{gathered}
2 \pi=6.2831853 \ldots \quad \frac{1}{2 \pi}=0.15915494 \ldots \\
\frac{180^{\circ}}{\pi}=57.295779 \ldots \approx 60^{\circ} \quad \frac{\pi}{180^{\circ}}=0.017453292 \ldots \approx \frac{1}{60^{\circ}} \\
\theta=\frac{s}{r} \quad \omega=\frac{d \theta}{d t}=\frac{v}{r} \quad \alpha=\frac{d^{2} \theta}{d t^{2}}=\frac{d \omega}{d t}=\frac{a}{r} \quad f=\frac{\omega}{2 \pi} \quad P=\frac{1}{f}=\frac{2 \pi}{\omega} \\
\omega=\alpha t+\omega_{0} \quad \Delta \theta=\frac{1}{2} \alpha t^{2}+\omega_{0} t \quad \omega^{2}=\omega_{0}^{2}+2 \alpha \Delta \theta \\
\Delta \theta=\frac{1}{2}\left(\omega_{0}+\omega\right) t \quad \Delta \theta=-\frac{1}{2} \alpha t^{2}+\omega t
\end{gathered}
$$

$$
\begin{gathered}
\vec{L}=\vec{r} \times \vec{p} \quad \vec{\tau}=\vec{r} \times \vec{F} \quad \vec{\tau}_{\text {net }}=\frac{d \vec{L}}{d t} \\
L_{z}=R P_{x y} \sin \gamma_{L} \quad \tau_{z}=R F_{x y} \sin \gamma_{\tau} \quad L_{z}=I \omega \quad \tau_{z, \text { net }}=I \alpha \\
I=\sum_{i} m_{i} R_{i}^{2} \quad I=\int R^{2} \rho d V \quad I_{\text {parallel axis }}=I_{\mathrm{cm}}+m R_{\mathrm{cm}}^{2} \quad I_{z}=I_{x}+I_{y} \\
I_{\mathrm{cyl} 1, \text { shell,thin }}=M R^{2} \quad I_{\mathrm{cyl}}=\frac{1}{2} M R^{2} \quad I_{\mathrm{cyl}, \text { shell,thick }}=\frac{1}{2} M\left(R_{1}^{2}+R_{2}^{2}\right) \\
I_{\mathrm{rod}, \text { thin }, \mathrm{cm}}=\frac{1}{12} M L^{2} \quad I_{\text {sph,solid }}=\frac{2}{5} M R^{2} \quad I_{\text {sph,shell,thin }}=\frac{2}{3} M R^{2} \\
a=\frac{g \sin \theta}{1+I /\left(m r^{2}\right)} \quad \\
K E_{\mathrm{rot}}=\frac{1}{2} I \omega^{2} \quad d W=\tau_{z} d \theta \quad P=\frac{d W}{d t}=\tau_{z} \omega
\end{gathered}
$$

$$
\Delta K E_{\mathrm{rot}}=W_{\mathrm{net}}=\int \tau_{z, \text { net }} d \theta \quad \Delta P E_{\mathrm{rot}}=-W=-\int \tau_{z, \mathrm{con}} d \theta
$$

$$
\Delta E_{\mathrm{rot}}=K E_{\mathrm{rot}}+\Delta P E_{\mathrm{rot}}=W_{\mathrm{non}, \mathrm{rot}} \quad \Delta E=\Delta K E+K E_{\mathrm{rot}}+\Delta P E=W_{\mathrm{non}}+W_{\mathrm{rot}}
$$

## 19 Static Equilibrium

$$
\begin{gathered}
\vec{F}_{\text {ext }, \text { net }}=0 \quad \vec{\tau}_{\text {ext,net }}=0 \quad \vec{\tau}_{\text {ext,net }}=\tau_{\text {ext,net }}^{\prime} \quad \text { if } F_{\text {ext,net }}=0 \\
0=F_{\text {net } x}=\sum F_{x} \quad 0=F_{\text {net } y}=\sum F_{y} \quad 0=\tau_{\text {net }}=\sum \tau
\end{gathered}
$$

20 Gravity

$$
\begin{gathered}
\vec{F}_{1 \text { on } 2}=-\frac{G m_{1} m_{2}}{r_{12}^{2}} \hat{r}_{12} \quad \vec{g}=-\frac{G M}{r^{2}} \hat{r} \quad \oint \vec{g} \cdot d \vec{A}=-4 \pi G M \\
P E=-\frac{G m_{1} m_{2}}{r_{12}} \quad V=-\frac{G M}{r} \quad v_{\text {escape }}=\sqrt{\frac{2 G M}{r}} \quad v_{\text {orbit }}=\sqrt{\frac{G M}{r}} \\
P^{2}=\left(\frac{4 \pi^{2}}{G M}\right) r^{3} \quad P=\left(\frac{2 \pi}{\sqrt{G M}}\right) r^{3 / 2} \quad \frac{d A}{d t}=\frac{1}{2} r^{2} \omega=\frac{L}{2 m}=\text { Constant }
\end{gathered}
$$

$$
R_{\text {Earth,mean }}=6371.0 \mathrm{~km} \quad R_{\text {Earth,equatorial }}=6378.1 \mathrm{~km} \quad M_{\text {Earth }}=5.9736 \times 10^{24} \mathrm{~kg}
$$

$$
R_{\text {Earth mean orbital radius }}=1.495978875 \times 10^{11} \mathrm{~m}=1.0000001124 \mathrm{AU} \approx 1.5 \times 10^{11} \mathrm{~m} \approx 1 \mathrm{AU}
$$

$$
R_{\text {Sun,equatorial }}=6.955 \times 10^{8} \approx 109 \times R_{\text {Earth,equatorial }} \quad M_{\text {Sun }}=1.9891 \times 10^{30} \mathrm{~kg}
$$

## 21 Fluids

$$
\rho=\frac{\Delta m}{\Delta V} \quad p=\frac{F}{A} \quad p=p_{0}+\rho g d_{\mathrm{depth}}
$$

$$
\text { Pascal's principle } \quad p=p_{\mathrm{ext}}-\rho g\left(y-y_{\mathrm{ext}}\right) \quad \Delta p=\Delta p_{\mathrm{ext}}
$$

Archimedes principle $\quad F_{\text {buoy }}=m_{\text {fluid dis }} g=V_{\text {fluid dis }} \rho_{\text {fluid }} g$
equation of continuity for ideal fluid $\quad R_{V}=A v=$ Constant
Bernoulli's equation $\quad p+\frac{1}{2} \rho v^{2}+\rho g y=$ Constant

## 22 Oscillation

$$
\begin{gathered}
P=f^{-1} \quad \omega=2 \pi f \quad F=-k x \quad P E=\frac{1}{2} k x^{2} \quad a(t)=-\frac{k}{m} x(t)=-\omega^{2} x(t) \\
\omega=\sqrt{\frac{k}{m}} \quad P=2 \pi \sqrt{\frac{m}{k}} \quad x(t)=A \cos (\omega t)+B \sin (\omega t) \\
E_{\text {mec total }} \\
=\frac{1}{2} m v_{\max }^{2}=\frac{1}{2} k x_{\max }^{2}=\frac{1}{2} m v^{2}+\frac{1}{2} k x^{2} \\
P=2 \pi \sqrt{\frac{I}{m g r}} \quad P=2 \pi \sqrt{\frac{r}{g}}
\end{gathered}
$$

23 Waves

$$
\begin{gathered}
\frac{d^{2} y}{d x^{2}}=\frac{1}{v^{2}} \frac{d^{2} y}{d t^{2}} \quad v=\sqrt{\frac{F_{\mathrm{T}}}{\mu}} \quad y=f(x \mp v t) \\
y=y_{\max } \sin [k(x \mp v t)]=y_{\max } \sin (k x \mp \omega t)
\end{gathered}
$$

$$
\text { Period }=\frac{1}{f} \quad k=\frac{2 \pi}{\lambda} \quad v=f \lambda=\frac{\omega}{k} \quad P \propto y_{\max }^{2}
$$

$$
\begin{gathered}
y=2 y_{\max } \sin (k x) \cos (\omega t) \quad n=\frac{L}{\lambda / 2} \quad L=n \frac{\lambda}{2} \quad \lambda=\frac{2 L}{n} \quad f=n \frac{v}{2 L} \\
v=\sqrt{\left(\frac{\partial P}{\partial \rho}\right)_{S}} \quad n \lambda=d \sin (\theta) \quad\left(n+\frac{1}{2}\right) \lambda=d \sin (\theta) \\
I=\frac{P}{4 \pi r^{2}} \quad \beta=(10 \mathrm{~dB}) \times \log \left(\frac{I}{I_{0}}\right) \\
f=n \frac{v}{4 L}: n=1,3,5, \ldots \quad f_{\text {medium }}=\frac{f_{0}}{1-v_{0} / v_{\text {medium }}} \\
f^{\prime}=f\left(1-\frac{v^{\prime}}{v}\right) \quad f=\frac{f^{\prime}}{1-v^{\prime} / v}
\end{gathered}
$$

## 24 Thermodynamics

$$
\begin{aligned}
& d E=d Q-d W=T d S-p d V \\
& T_{\mathrm{K}}=T_{\mathrm{C}}+273.15 \mathrm{~K} \quad T_{\mathrm{F}}=1.8 \times T_{\mathrm{C}}+32^{\circ} \mathrm{F} \\
& Q=m C \Delta T \quad Q=m L \\
& P V=N k T \quad P=\frac{2}{3} \frac{N}{V} K E_{\mathrm{avg}}=\frac{2}{3} \frac{N}{V}\left(\frac{1}{2} m v_{\mathrm{RMS}}^{2}\right) \\
& v_{\mathrm{RMS}}=\sqrt{\frac{3 k T}{m}}=2735.51 \ldots \times \sqrt{\frac{T / 300}{A}} \\
& P V^{\gamma}=\text { constant } \\
& 1<\gamma \leq \frac{5}{3} \quad v_{\text {sound }}=\sqrt{\frac{B}{\rho}}=\sqrt{\frac{-V(\partial P / \partial V)_{S}}{m(N / V)}}=\sqrt{\frac{\gamma k T}{m}} \\
& \varepsilon=\frac{W}{Q_{\mathrm{H}}}=\frac{Q_{\mathrm{H}}-Q_{\mathrm{C}}}{W}=1-\frac{Q_{\mathrm{C}}}{Q_{\mathrm{H}}} \\
& \eta_{\text {heating }}=\frac{Q_{\mathrm{H}}}{W}=\frac{Q_{\mathrm{H}}}{Q_{\mathrm{H}}-Q_{\mathrm{C}}}=\frac{1}{1-Q_{\mathrm{C}} / Q_{\mathrm{H}}}=\frac{1}{\varepsilon} \quad \eta_{\text {cooling }}=\frac{Q_{\mathrm{C}}}{W}=\frac{Q_{\mathrm{H}}-W}{W}=\frac{1}{\varepsilon}-1=\eta_{\text {heating }}-1 \\
& \varepsilon_{\text {Carnot }}=1-\frac{T_{\mathrm{C}}}{T_{\mathrm{H}}} \quad \eta_{\text {heating,Carnot }}=\frac{1}{1-T_{\mathrm{C}} / T_{\mathrm{H}}} \quad \eta_{\text {cooling, Carnot }}=\frac{T_{\mathrm{C}} / T_{\mathrm{H}}}{1-T_{\mathrm{C}} / T_{\mathrm{H}}}
\end{aligned}
$$

